





Materiali e tipologie costruttive

EN1998-1-2. Strutture metalliche e composte acciaio-cls

Raffaele Landolfo, Università degli Studi di Napoli Federico II

Contents

- Introduction
- Specific rules for steel buildings
- Specific rules for composite steel-concrete buildings
- Specific rules for aluminum buildings
- Conclusions

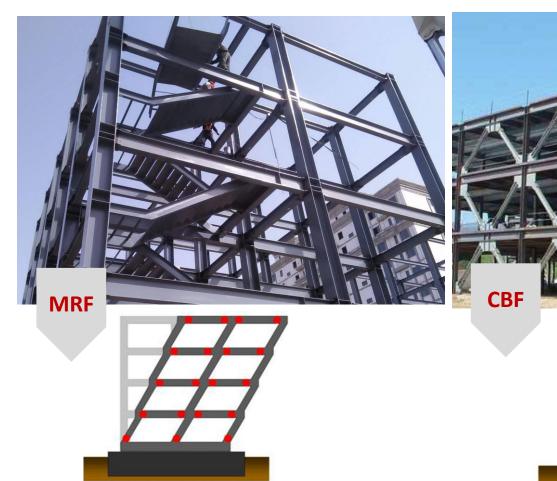
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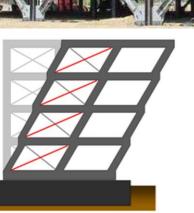
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Introduction

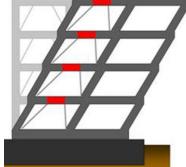
Seismic-resistant steel structural typologies









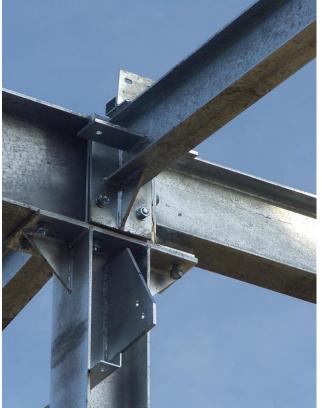


Introduction

Steel connections









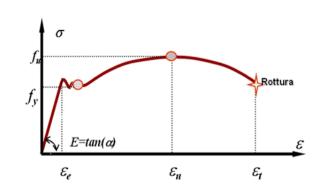
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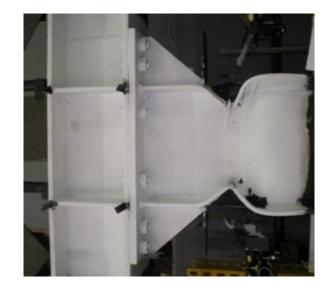
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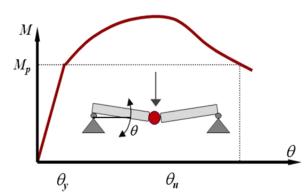
Benefits of steel in seismic design: Ductility

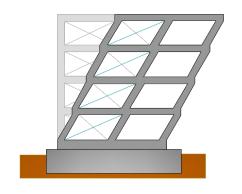


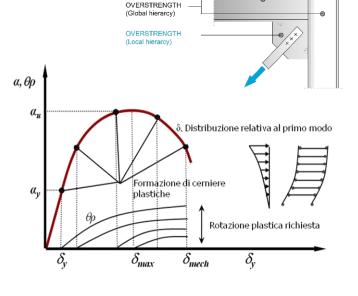












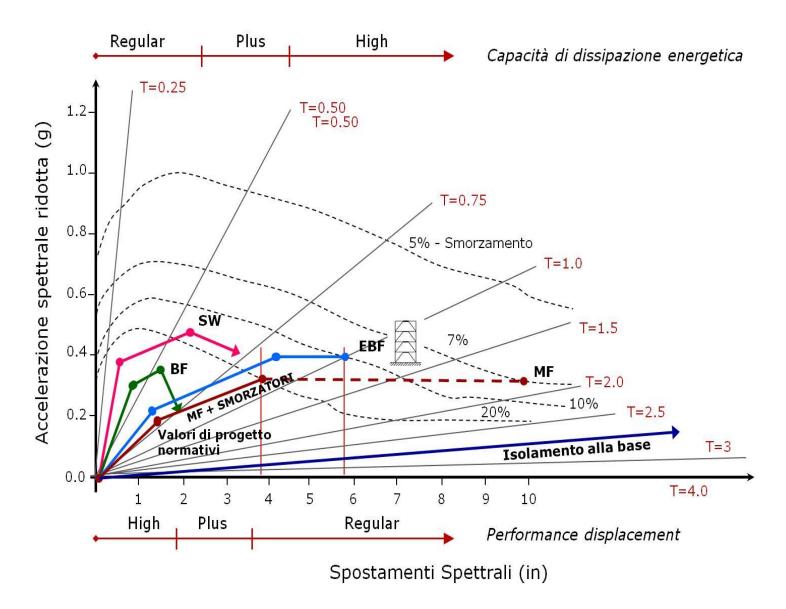
Material Ductility

Member Ductility

System Ductility

Introduction

Seismic performance of steel structures in seismic areas



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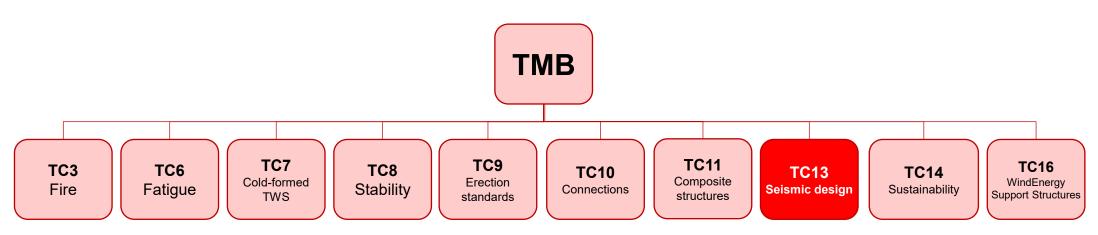
Introduction

ECCS Technical Committes

 The expert forum that establishes <u>consensus on European practice</u> and provides the <u>undisputed background for normalization</u>;



- The expert forum that identifies ongoing developments in specific fields;
- The expert forum that helps establishing priorities for R&DI.



ECCS Technical Committees comprise over 200 experts

Introduction

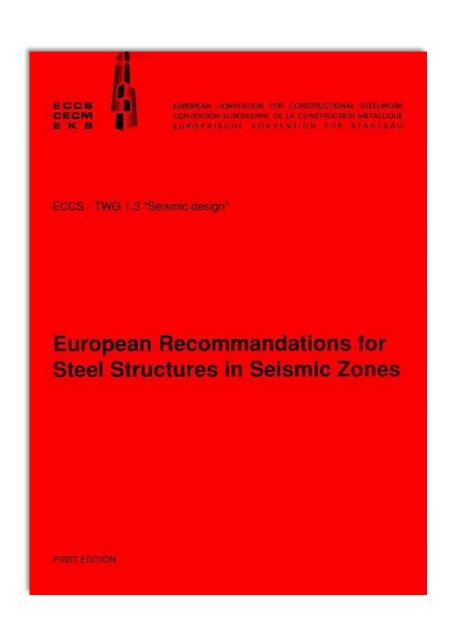
ECCS- TC13 Seismic Design Committee

Genesis of EU seismic codes

The development of seismic design provisions for steel structures is ongoing for over forty years in the framework of ECCS.

- First activities started in 1980's
- First EU seismic code:

ECCS code 1991 "European for Recommendations for Steel Structures in Seismic Zones".



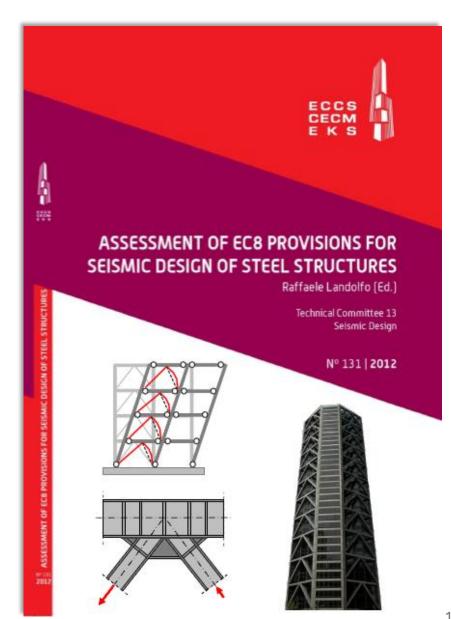
Introduction

The activity of TC13

Since **2007** TC13 worked to **improve the rules on seismic design of steel structures.**

In 2013 "Assessment of EC8 Provisions for Seismic Design of Steel Structures" was published, containing a critical and systematic review of current EC8 and identifying main criticisms and issues needing revisions and/or upgrading.

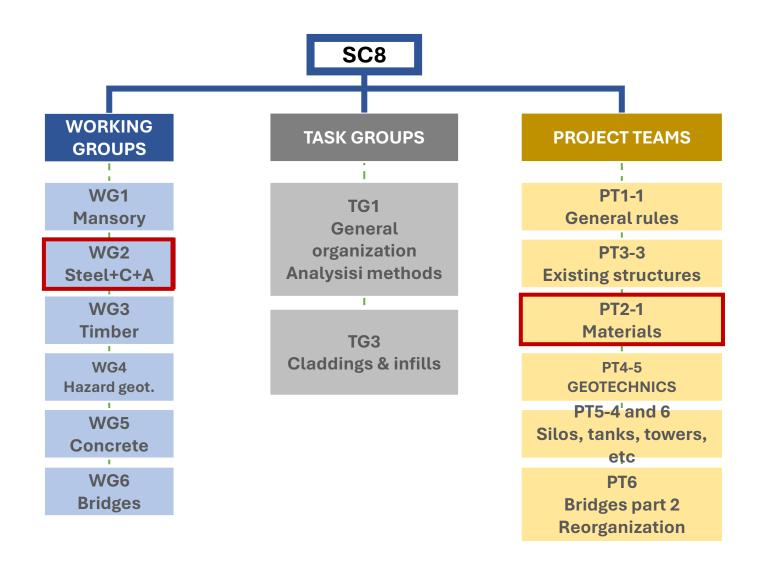
- Material overstrength
- Selection of steel of toughness
- Local ductility
- Design rules for connections in dissipative zones
- New links in eccentrically braced frames
- Behaviour factors
- Capacity-design rules
- Design of concentrically braced frames
- Dual structures
- Drift limitations and second-order effects
- New structural types
- Low-dissipative structures



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Introduction

Organisation of CEN/TC250/SC8



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- Specific rules for steel buildings
- Specific rules for composite steel-concrete buildings
- Specific rules for aluminum buildings
- Conclusions

2025

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Specific rules for steel buildings

Ref. No. EN 1998-1:2004: E

Evolution of seismic rules

EC8 1ST GENERATION

EN1998-1 **EUROPEAN STANDARD** NORME EUROPÉENNE (2004)EUROPÄISCHE NORM ICS 91.120.25 Supersedes ENV 1998-1-1:1994, ENV 1998-1-2:1994. English version Eurocode 8: Design of structures for earthquake resistance -Part 1: General rules, seismic actions and rules for buildings Eurocode 8: Calcul des structures pour leur résistance aux séismes - Partie 1: Règles générales, actions sismiques et Eurocode 8: Auslegung von Bauwerken gegen Erdbeben -Teil 1: Grundlagen, Erdbebenenwirkungen und Regeln für Hochbauten règles pour les bâtiments This European Standard was approved by CEN on 23 April 2004. CEN members are bound to comply with the CEN/CENELEC Internal Regulations which stipulate the conditions for giving this European Standard the status of a national standard without any alteration. Up-to-date lists and bibliographical references concerning such national standards may be obtained on application to the Central Secretariat or to any CEN member. This European Standard exists in three official versions (English, French, German). A version in any other language made by translation under the responsibility of a CEN member into its own language and notified to the Central Secretariat has the same status as the official CEN members are the national standards bodies of Austria, Belgium, Cyprus, Czech Republic, Denmark, Estonia, Finland, France, Germany, Greece, Hungary, Iceland, Ireland, Italy, Latvia, Lithuania, Luxembourg, Malta, Netherlands, Norway, Poland, Portugal, Slovakia, Slovenia, Spain, Sweden, Switzerland and United Kingdom. EUROPÄISCHES KOMITEE FÜR NORMUNG Management Centre: rue de Stassart, 36 B-1050 Brussels

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VS

Eurocode 8: Design of structures for earthquake resistance.

Part 1. General rules, seismic actions and rules for buildings

EC8 2ND GENERATION

EN1998-1-2 (2025)

CEN/TC 250

Date: 2025-02-13

FprEN 1998-1-2:2025

Secretariat: BSI

Eurocode 8 — Design of structures for earthquake resistance — Part 1-2: Buildings

Eurocode 8 – Auslegung von Bauwerken gegen Erdbeben – Teil 1-2: Hochbauten Eurocode 8 – Calcul des structures pour leur résistance au séisme – Part 1-2 :

ICS:

Eurocode 8: Design of structures for earthquake resistance.

Part 1-2: Buildings

1

EC8 1st Generation



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EC8 2nd Generation



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EN1998-1 (2004) – Chapter 6 Chapter 6 of EN1998-1 has 23 pages

EN1998-1-2 (2025) - Chapter 11 **Chapter 11 of EN1998-1-2** has 49 pages

Evolution of seismic rules

STEEL CHAPTER EC8 1ST GENERATION EN 1998-1 (2004) Chapter 6 VS

EC8 2ND GENERATION EN 1998-1-2 (2025) Chapter 11

- Introduction of new design rules for low-moderate/medium ductility (DC2);
- Introduction of new structural types;
- Improvement of seismic design rules for traditional types;
- New Annexes

MAIN NOVELTIES

EN1998-1 (2004) - Chapter 6

Structural systems:

MRFs
CBFs
EBFs
Dual Frames

EN1998-1-2 (2025) - Chapter 11

Structural systems:

MRFs
CBFs
EBFs
BRBFs
Dual Frames
Light weight structures

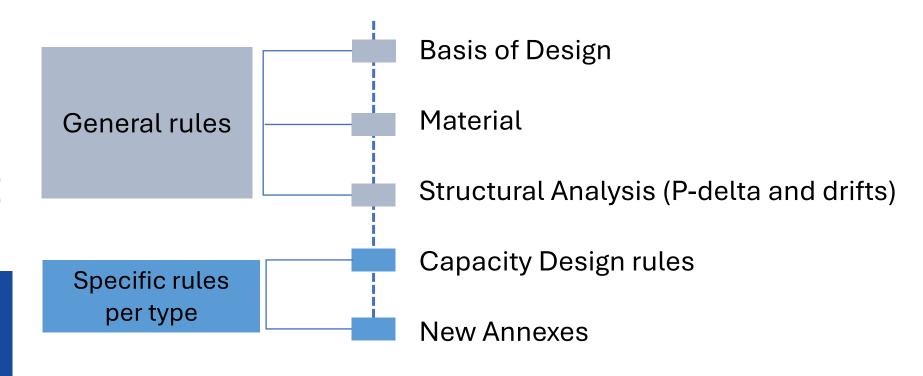
EN1998-1 (2004) – Chapter 6 NO ANNEXES

EN1998-1-2 (2025) - Chapter 11

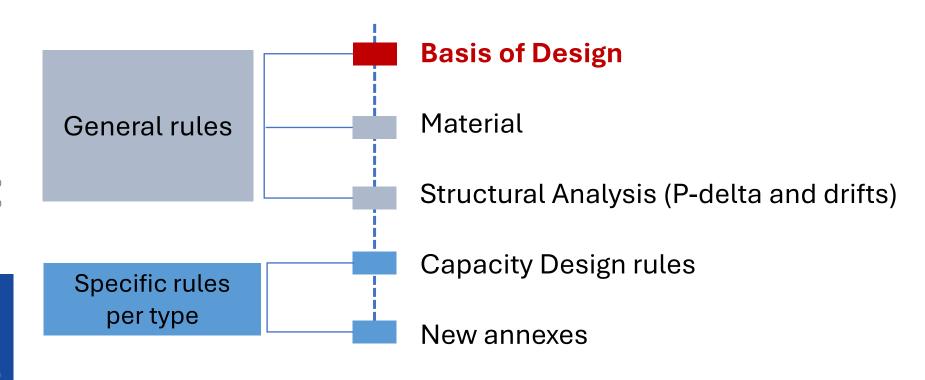
Annexes

- E Seismic design of connections for steel buildings
- F Steel light weight structures
- H Seismic design of exposed and embedded steel and composite column base connections

Addressed topics



Addressed topics



Basis of Design: Structural Types

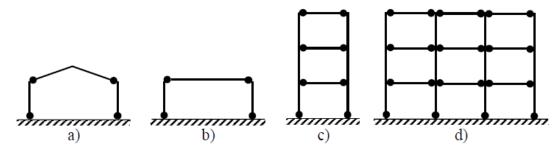


Figure 11.1 — Moment resisting frames (dissipative zones in beams and at bottom of columns): a) portal frame; b) single-storey MRF; c) single-span multi-storey MRF; d) multi-span multi-storey MRF

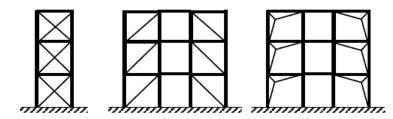


Figure 11.2 — Frames with concentric bracings where the concept of tension-only diagonals is allowed

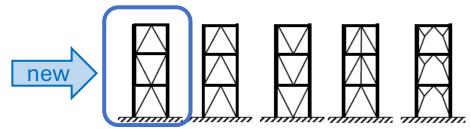


Figure 11.3 — Frames with concentric bracings where the concept of tension-compression diagonals is mandatory

Basis of Design: Structural Types

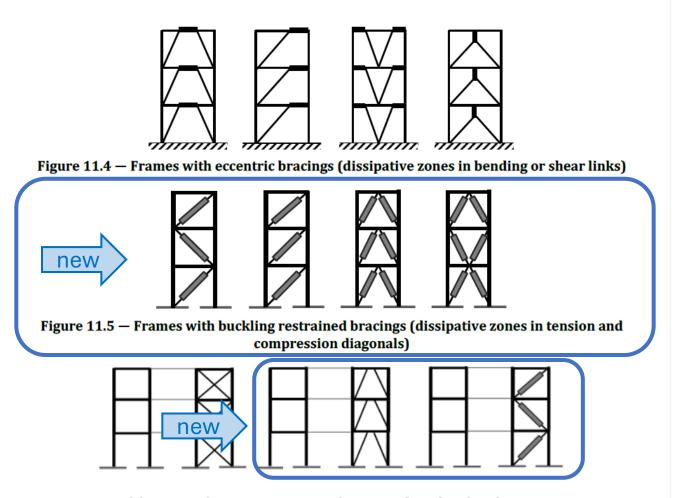


Figure 11.6 — Dual frames with moment resisting frame combined with either concentric, eccentric or buckling restrained bracing (dissipative zones in both moment and braced frames)

Basis of Design: Structural Types

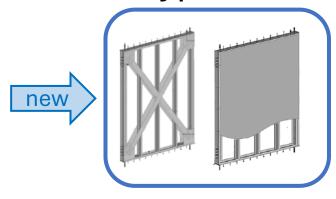


Figure 11.7 — Lightweight steel systems: a) Strap braced walls; b) Shear walls with steel sheet or wood sheathing or gypsum sheathing

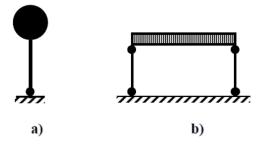


Figure 11.8 — Inverted pendulum: a) dissipative zones at the column base; b) dissipative zones in columns $(N_{\rm Ed,G}/N_{\rm pl,Rd} \ge 0.3)$

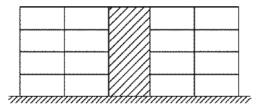
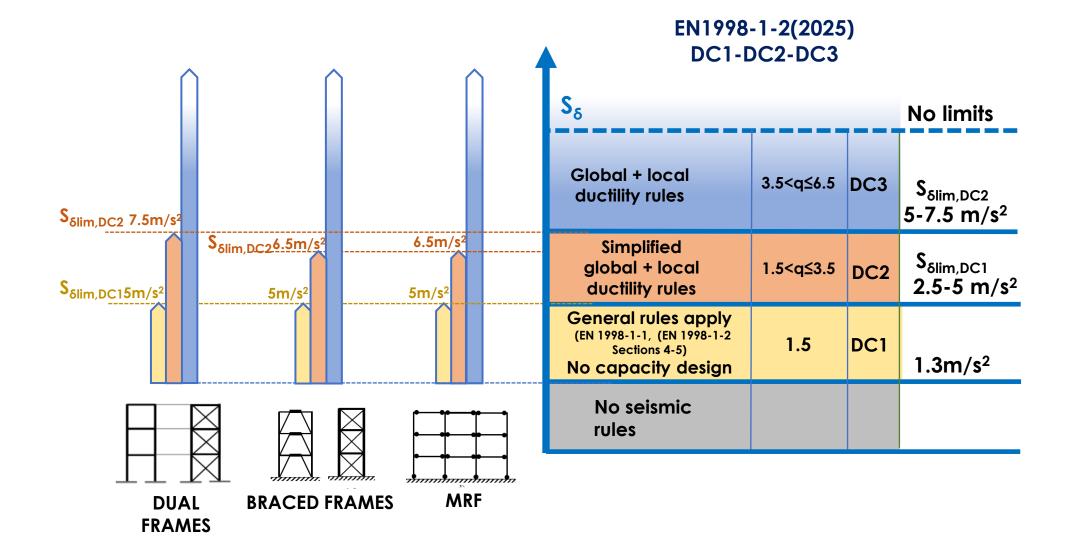


Figure 11.9 - Structures with concrete cores or concrete walls

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Specific rules for steel buildings

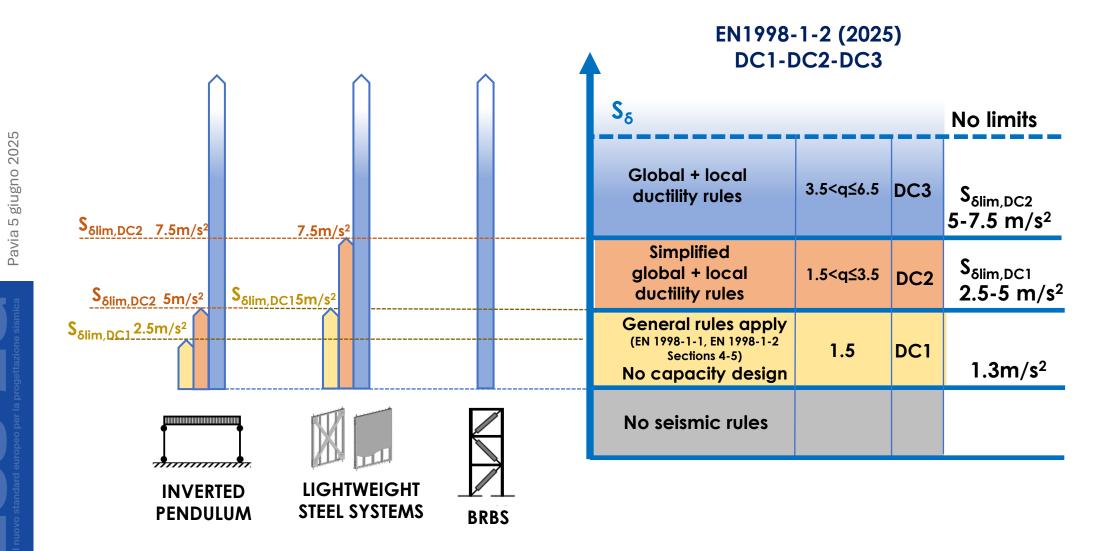
Basis of Design: limits of seismic action



Il nuovo standard europeo per la progettazione sismic

Specific rules for steel buildings

Basis of Design: limits of seismic action



Il nuovo standard europeo per la progettazione sism

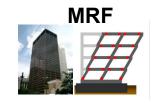
Specific rules for steel buildings

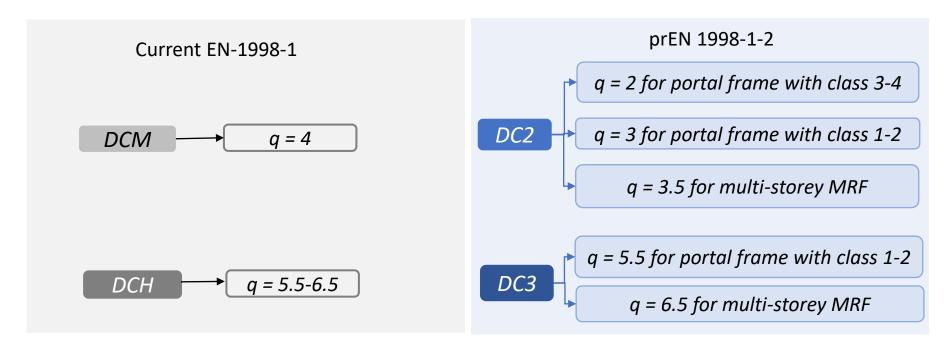
Basis of Design: behaviour factors

	Ductility Class						
STRUCTURAL TYPE	DC2				DC3		
	$q_{ m D}$	$q_{ m R}$	q	$q_{\scriptscriptstyle m D}$	$q_{ m R}$	q	
a) Moment resisting frames (MRFs)							
Portal frames and single-storey MRFs with class 3 and 4 cross sections	1,3	1	2	-	-	-	
Portal frames and single-storey MRFs with class 1 and 2 cross sections	1,8	1,1	3	3,3	1,1	5,5	
Multi-storey MRFs	1,8	1,3	3,5	3,3	1,3	6,5	
b) Frames with concentric bracings							
Diagonal bracings	1,7	1	2,5	2,4	1,1	4	
V-bracings	1,/	1	2,3	2,4	1,1	4	
X-bracings on either single or two-storey							
c) Frames with eccentric bracings	1,8	1,3	3,5	3,1	1,3	6	
d) Frames with buckling restrained braces				3,3	1,2	6	
e) Dual frames							
MRFs with concentric bracing	1,8	1,1	3	2,9	1,1	4,8	
MRFs with eccentric bracing	2,1	1,3	4	3,3	1,3	6,5	
MRFs with buckling restrained braces	-	-	-	3,3	1,3	6,5	
f) Structures with concrete cores or concrete walls		See 10					
g) Lightweight steel frame wall systems							
with flat strap bracing	1,3	1	2	1,7	1	2,5	
with steel sheeting	1,3	1	2	1,7	1	2,5	
with wood sheathing	1,3	1	2	1,7	1	2,5	
with gypsum sheathing	1,1	1	1,7	1,3	1	2	
h) Inverted pendulum	1,3	1	2	1,5	1	2,3	
i) Moment resisting frames with infills	ļ	ļ		ļ	ļ		
Unconnected concrete or masonry infills, in contact with the frame	2	1	3				
Connected reinforced concrete infills		See 10					
Infills isolated from moment frame		(see MRFs)					

Basis of Design: behaviour factors

EN-1998-1 (2004) VS EN 1998-1-2 (2025)

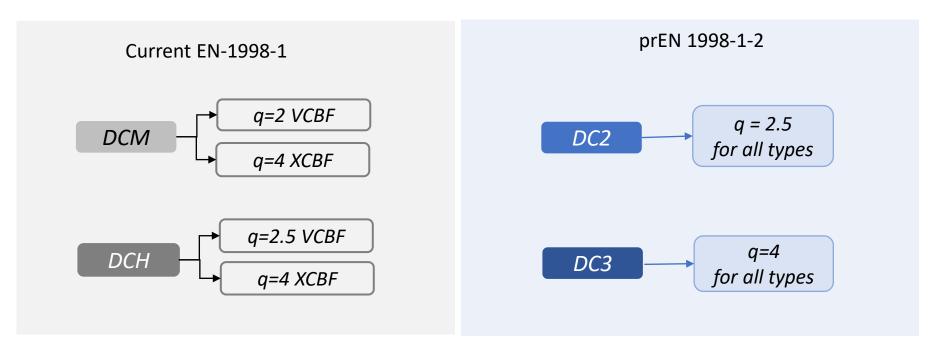




Basis of Design: behaviour factors

Current EN-1998-1 VS prEN 1998-1-2

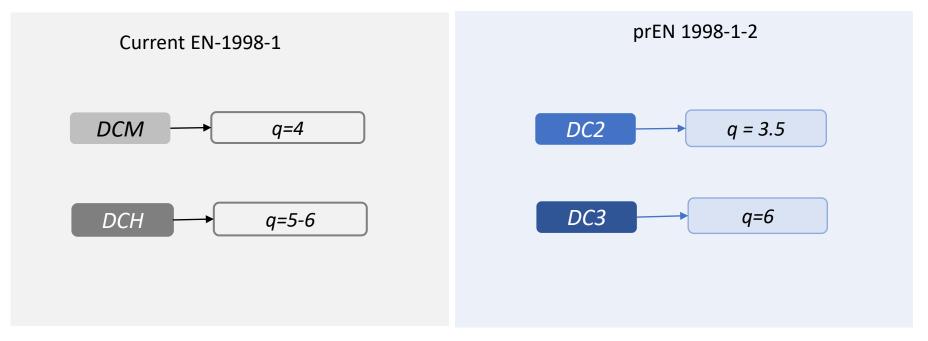




Basis of Design: behaviour factors

EN-1998-1 (2004) VS EN 1998-1-2 (2025)

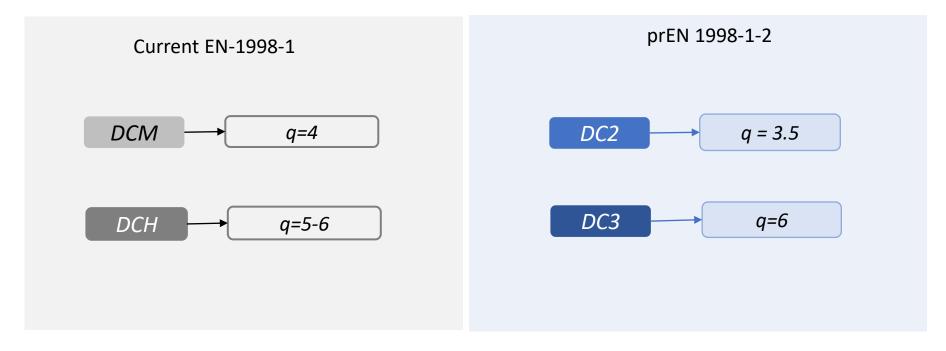




Basis of Design: behaviour factors

EN-1998-1 (2004) VS EN 1998-1-2 (2025)





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Specific rules for steel buildings

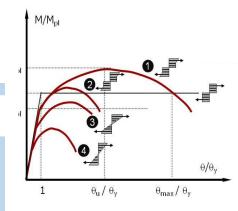
Basis of Design: required cross sectional classes

EN1998-1 (2004)

DCH	2.5 <q≤6.5< th=""><th>Class 1</th></q≤6.5<>	Class 1
DCM	2 <q≤3.5< td=""><td>Class 1, 2</td></q≤3.5<>	Class 1, 2

EN1998-1-2 (2025)

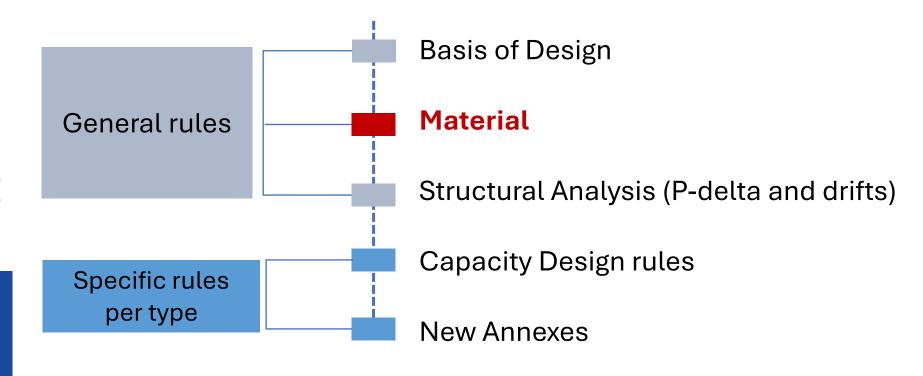
	DC3	q>3.5	Class 1
		2≤q≤2.5	Class 1, 2, 3 or 4 for lightweight systems
	DC2	1.5 <q≤2< td=""><td>Class 1, 2, 3 or 4 for portal frames, lightweight systems and single storey MRF</td></q≤2<>	Class 1, 2, 3 or 4 for portal frames, lightweight systems and single storey MRF
		1.5 <q≤2< td=""><td>Class 1, 2 for inverted pendulum</td></q≤2<>	Class 1, 2 for inverted pendulum
		2 <q≤3.5< td=""><td>Class 1, 2 for MRFs, CBFs, EBFs and Dual frames</td></q≤3.5<>	Class 1, 2 for MRFs, CBFs, EBFs and Dual frames



REQUIRED CROSS
SECTIONAL CLASS
DEPENDS ON
STRUCTURAL TYPES

CLASSES 3 and 4 are allowed for certain structural typologies

Addressed topics



Material: random variability of steel strength

EN1998-1 (2004)

 γ_{ov} is the material overstrength factor used in design

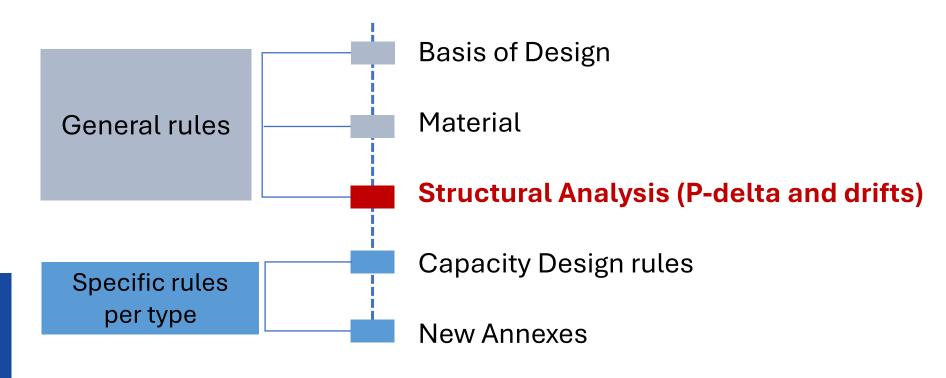
NPD-Recommended Value 1,25

EN1998-1-2 (2025)

 ω_{rm} is the ratio between the expected (i.e. average) yield strength $f_{y,average}$ and the relevant f_y . This ratio is the material overstrength factor used in design, which depends on the steel grade

Steel grade	$\begin{array}{c} \textbf{Material randomness} \\ \textbf{coefficient } \omega_{\text{rm}} \end{array}$
S235	1.45
S275	1.35
S355	1.25
S420	1.25
S460	1.2

Addressed topics

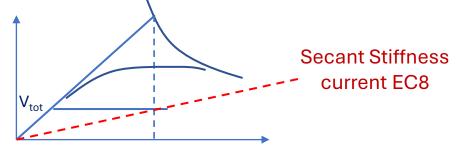


Structural analysis: second order effects

Current EN-1998 (2005)

Stability coefficient based on the secant stiffness of the idealized elastic-plastic response curve, which disregards the design overstrength and the plastic distribution (i.e. redundancy)

$$\theta = \frac{P_{tot} \cdot d_r}{V_{tot} \cdot h}$$



EN1998-1-2(2025)

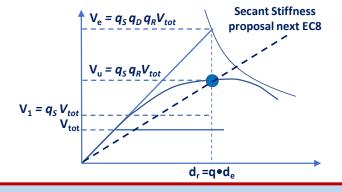
Modified stability coefficient based, which account for design overstrength and the plastic

distribution

$$\theta = \frac{P_{tot} \cdot d_{r,SD}}{q_{s} \cdot q_{R} \cdot V_{tot} \cdot h}$$

for DC2
$$\rightarrow q_s = 1.5$$

for DC3
$$\rightarrow q_s = \omega_{rm} \Omega_d$$



Structural analysis: drift limitation

Current EN-1998(2005)

At Damage Limitation state the interstorey drift should be verified as follows

$$d_r \leq \alpha h$$

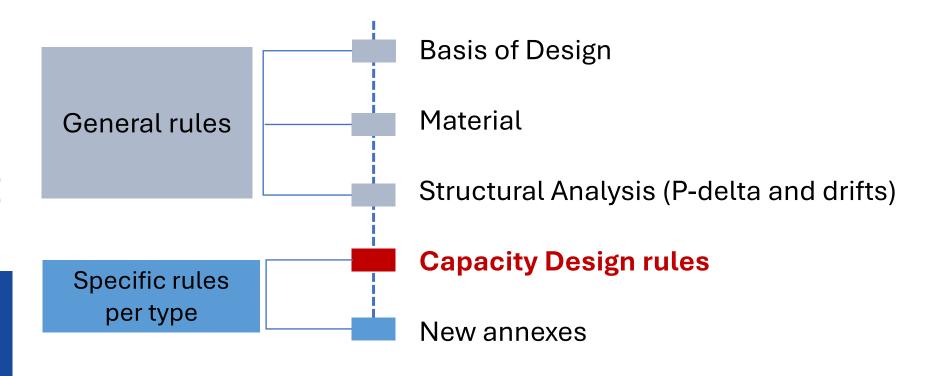
where $\alpha = 0.05$; 0.075; 0.01 depeding on the non-structural elements

No mandatory check at Damage Limitation. At Significant Damage limit state should be verified as follows:

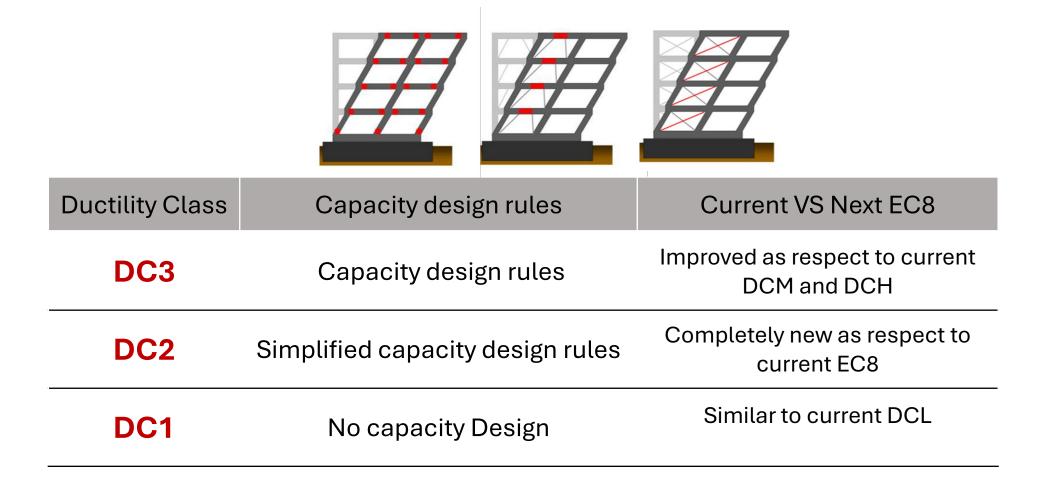
$$d_r \leq \lambda h$$

 λ depeds on the structural system: λ = 0.01 for lightweight systems; λ = 0.015 for braced frames and inverted pendulum λ = 0.02 for dual and MRFs

Addressed topics



Capacity design: general rules



Capacity design: general rules

EN1998-1 (2004) DCM

$R_d \geq E_{Ed,G} + 1.1 \cdot \gamma_{ov} \cdot \Omega \cdot E_{Ed,E}$

$$\Omega = \min \left(\frac{R_d}{E_{Ed,E}} \right)$$

EN1998-1-2 (2025) DC2

$$M_{Rd} \ge M_{Ed,G}" + "M_{Ed,E}$$

$$V_{Rd} \ge V_{Ed,G}$$
" + " $V_{Ed,E}$

$$N_{Rd} \geq N_{Ed,G}" + "\Omega \cdot N_{Ed,E}$$

 Ω = seismic action magnification factor (from the Table 11.7)

In current DCM all seismic induced effects are magnified In new DC2 only axial forces are magnified

Table 11.7 — Members to which (1) or (2) apply. Values of seismic action magnification factor Ω in DC2

STRUCTURAL TYPE	Ω	Members to which (1) or (2) apply
Moment resisting frames (MRFs)		
Portal frames with class 3 and 4 cross sections	1,5	
Single-storey MRFs with class 3 and 4 cross sections	1,5	columns
Portal frames and single-storey MRFs with class 1 and 2 cross sections	1,7	
Multi-storey MRFs	2	
MRFs with friction connections	2	
Frames with concentric bracings		
Diagonal bracings	1.5	beams and columns
V-bracings		
X-bracings on either single or two-storey		
Frames with eccentric bracings	2	beams outside the link, braces and columns
Dual frames		braces and columns
Dual Hames		beams and columns of
		the concentric bracing;
MRFs with concentric bracing	1,7	
		columns of the MRF;
		beams out of the link,
MRFs with eccentric bracing	2	braces and columns of
MRY'S WITH ECCENTRIC DIACTING		the eccentric bracing;
Structures with concrete cores or concrete walls	See 10	columns of the MRF
	See 10	
Lightweight steel frame wall systems	1.5	
with flat strap bracing	1,5	connections and framing: chord studs and tracks
with steel sheeting	1,5	
with wood sheathing	1,5	
with gypsum sheathing	1,3	1
Inverted pendulum structures	1,5	columns
Moment resisting frames with infills		,
with unconnected with non-interacting concrete or masonry infills	1,5	columns
with connected reinforced concrete infills	See 10	See section 10
with non-interacting infills	(see MRFs)	columns

Il nuovo standard europeo per la prodettazione sismica

Specific rules for steel buildings

Capacity design: general rules

EN1998-1 (2004) DCH

$$R_d \ge E_{Ed,G} + 1.1 \cdot \gamma_{ov} \cdot \Omega \cdot E_{Ed,E}$$

Ω Design overstrength of dissipative members

EN1998-1-2 (2025) DC3

$$R_d \ge E_{Ed,G} + \omega_{rm} \cdot \omega_{sh} \cdot \Omega_d \cdot E_{Ed,E}$$

 Ω_d Design overstrength of dissipative members

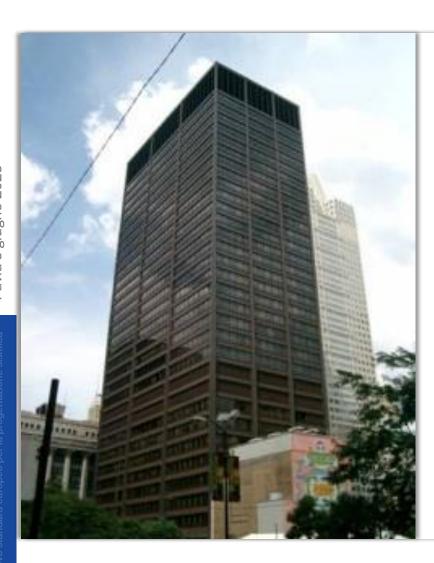
 ω_{sh} hardening overstrength factor

 ω_{rm} material randomness coefficient

In new DC3 the hardening factor is specified per dissipative mechanism

Table 11.8 — Overstrength factor $\omega_{\rm sh}$ accounting for hardening of the dissipative zones

Structural Type	Dissipative Zones	Plastic Mechanism	$\omega_{ m sh}$
Moment resisting frames	beams yielding connections columns at base	bending	$\frac{\left(f_{y}+f_{u}\right)}{2f_{y}} \le 1.2$
	friction connections	friction	$1,3\omega_{\rm sr}\omega_{\mu} \leq 2,2$ $\omega_{\rm sr}$ and ω_{μ} as defined in Annex E
Frames with concentric	diagonal members	axial	1,1
bracings (simple and dual)	all members	bending (see 11.10.5 and 11.10.6)	1,1
oracings (simple and duar)	dissipative	axial	1,1
	connections	bending	1,2
		shear	1,5
Frames with eccentric bracings (simple and dual) long links beams - colum	short links	shear $e \leq M_{\rm p,link}/V_{\rm p,link}$ (very short links)	1,8
	SHOPT HINKS	shear $M_{ m p,link}/V_{ m p,link} < e \le 1,6 M_{ m p,link}/V_{ m p,link}$ (short links)	1,5
	intermediate	bending and shear $e \le 2,6M_{\rm p,link}/V_{\rm p,link}$	1,5
	links	bending and shear $2.6M_{\rm p,link}/V_{\rm p,link} \le e \le 3M_{\rm p,link}/V_{\rm p,link}$	1,35
		Bending $3M_{\rm p,link}/V_{\rm p,link} \le e \le 5M_{\rm p,link}/V_{\rm p,link}$	1,25
	long links	Bending $e > 5M_{ m p,link}/V_{ m p,link}$	$\omega_{\rm sh} = \frac{\left(f_{\rm y} + f_{\rm u}\right)}{2f_{\rm y}} \le 1,2$
	beams - columns	bending (see 11.11.5)	1,1
Frames with buckling	diagonal members	axial	see 11.12.3(4)
restramed braces	beams - columns	bending (see 11.12.6)	1,2



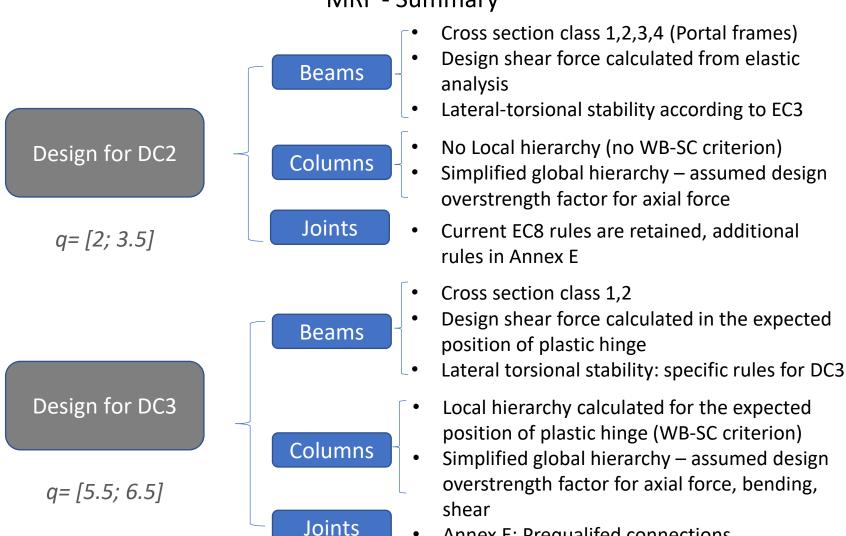
SPECIFIC RULES FOR MOMENT RESISTING FRAMES

1ST VS 2ND GENERATION: main novelties

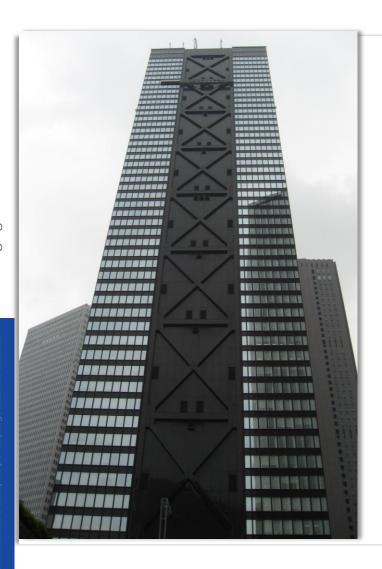
- Simplified hierarchy of resistances in DC2
- Expected location of plastic hinge is considered in calculations in DC3
- Specific rules for lateral-torsional stability in DC3
- Specific rules for columns in DC3
- Prequalification of beam-to-column joints

Capacity design

MRF - Summary



Annex E: Prequalifed connections

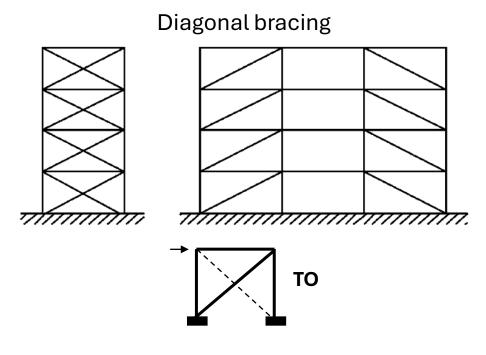


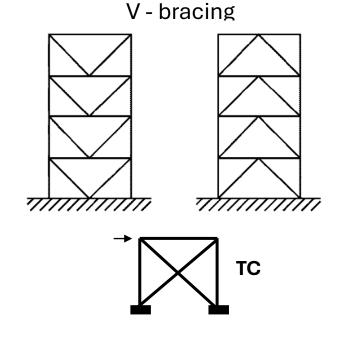
SPECIFIC RULES FOR CONCENTRICALLY BRACED FRAMES

1ST VS 2ND GENERATION: main novelties

- Simplified hierarchy of resistances in DC2
- Use of TC model for XCBFs
- New global slenderness limits
- Specific local slenderness limits for dissipative members in DC3
- Use of plastic mechanism analysis to determine required strength of non dissipative members in DC3
- Annex E for design of brace-to-frame connections in DC3

Frame with concentric bracing (CBF) in EN1998-1 (2004)





STRUCTURAL TYPE	Ductili	Ductility Class		
	DCM	DCH		
b) Frame with concentric bracings				
Diagonal bracings	4	4		
V-bracings	2	2,5		
		+		

Capacity design





Joints (gusset connections)

Both DC2 and DC3 shall comply with the similar requirements for brace connections. Specific rules are given in Annex E





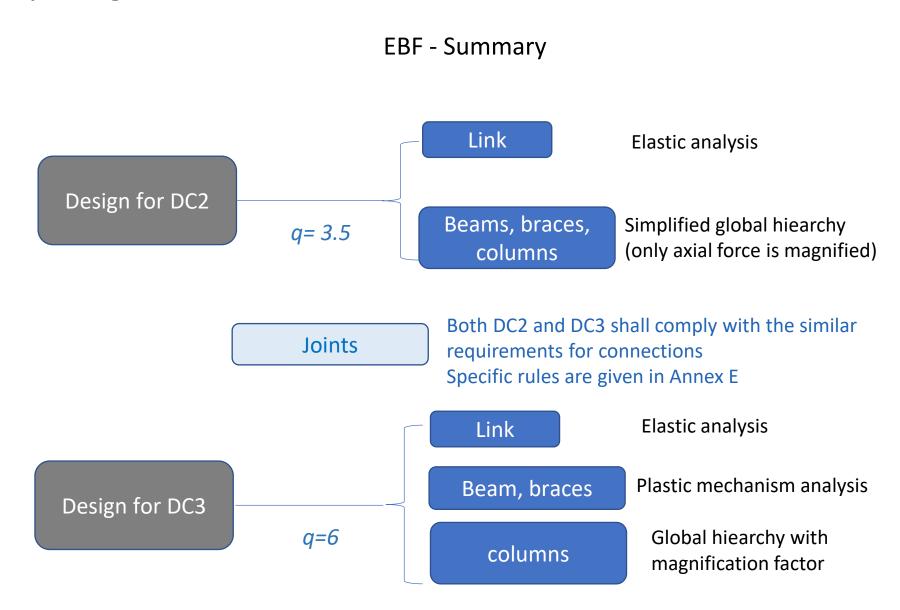
SPECIFIC RULES FOR ECCENTRICALLY BRACED FRAMES

1ST VS 2ND GENERATION: main novelties

- BOX sections allowed for links
- Simplified hierarchy of resistances in DC2
- No overstrength variation limit in DC2
- Use of plastic mechanism analyses to determine required strength of non dissipative members in DC3

Specific rules for steel buildings for steel buildings

Capacity design rules





SPECIFIC RULES FOR BUCKLING RESTRAINED BRACES

1ST VS 2ND GENERATION: main novelties

- BRBs design rules are INTRODUCED
- BRBs shall be designed solely in DC3
- Capacity design rules are provided

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Specific rules for steel buildings

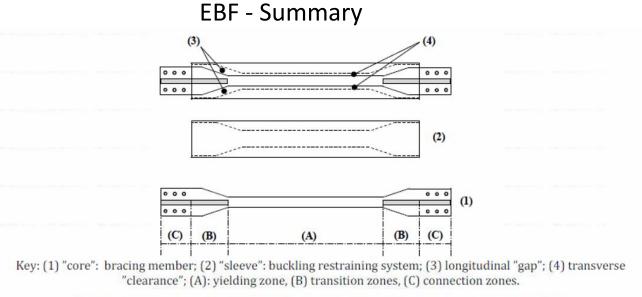
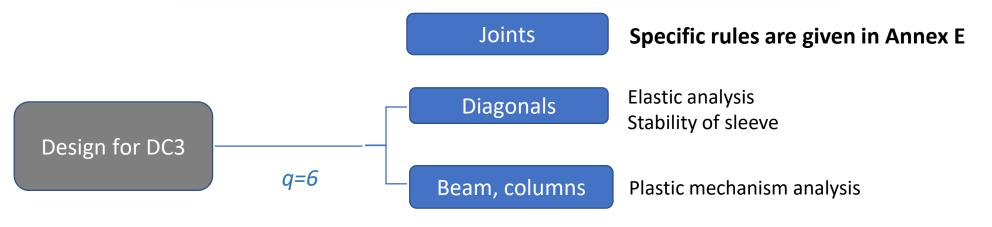
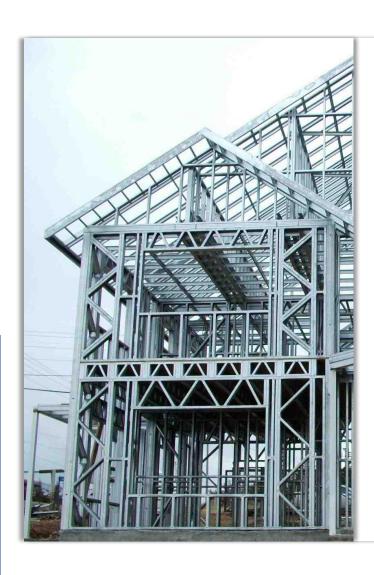


Figure 11.17 - Geometrical features and main components of a typical BRB



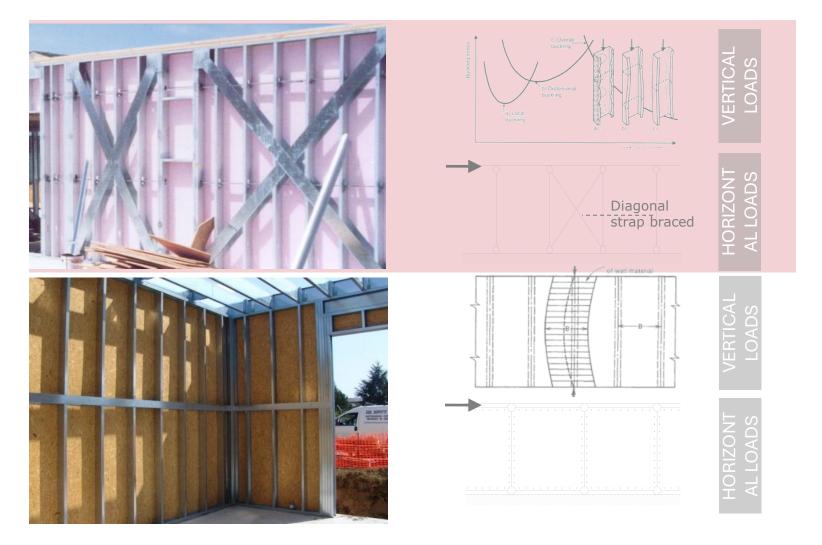


SPECIFIC RULES FOR LIGHTWEIGHT STEEL STRUCTURES

1ST VS 2ND GENERATION: main novelties

- LWSS design rules are INTRODUCED
- LWSS can be designed in all DC
- Capacity design rules are provided

Lightweight steel structures: Design approaches

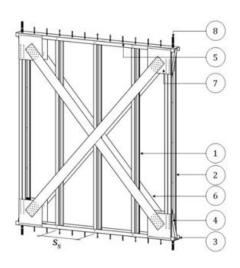


Strap braced walls design

Shear walls with sheetings design

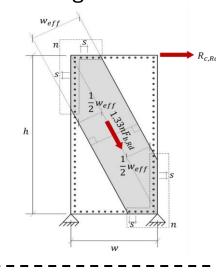
1. Strap-braced walls





2. Shear walls with steel sheet sheathing



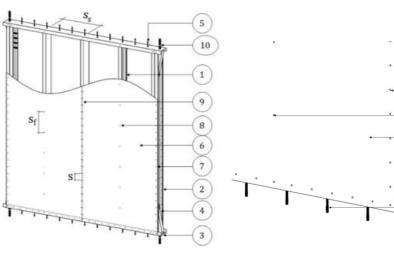


Shear walls with panels (wood, gypsum)



3. Shear walls with wood sheathing





4. Shear walls with gypsum sheathing

Seismic design criteria for CFS systems according to EN1998-1-2



All-steel structure



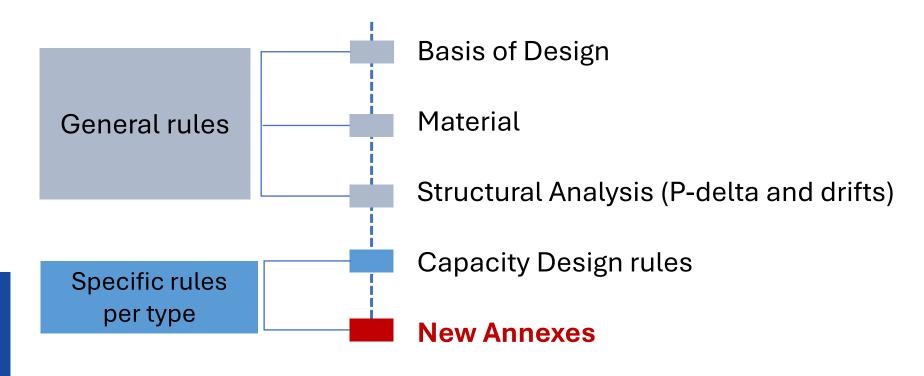
Tipologia strutturale	DC2	DC3	Design
	q	q	approach
Strutture con controventi a piatti	2	2.5	Dissipative

Shear walls with sheetings



Tipologia strutturale	DC2	DC3	Design
	q	q	approach
Strutture con lamiera d'acciaio	2	2.5	Dissipative
Strutture con pannelli di legno	2	2.5	Dissipative
Strutture con pannelli di cartongesso	1.7	2	Dissipative

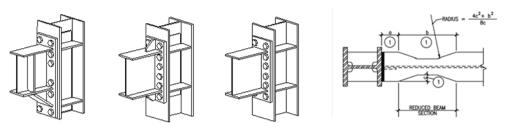
Addressed topics

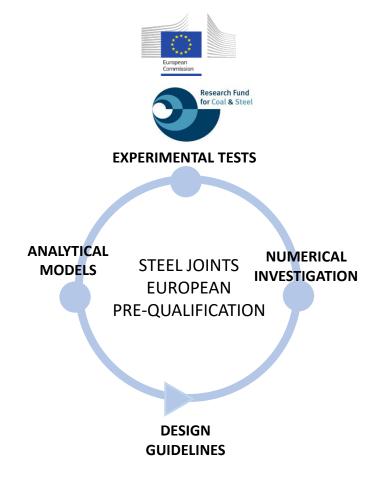


Background:

European Qualification of Seismic Resistant Steel Beam-to-column Joints

- The EQUALJOINTS research project aimed at providing prequalification procedure for a set of selected seismic resistant steel beam-to-column joints, introducing a codified practice currently missing in Europe.
- A large experimental programme supported by theoretical and numerical analyses has been performed
- The **guidelines** for the seismic design of joints developed within the Equaljoints project constitute the **scientific background** seismic rules given for beam.to-column joints in **the Annex E of EN 1998-1-2**.





More details in:

R. Landolfo, European seismic prequalification of steel beam-to-column joints: EQUALJOINTS and EQUALJOINTS-Plus projects, Journal of Constructional Steel Research 192 (2025) 107238

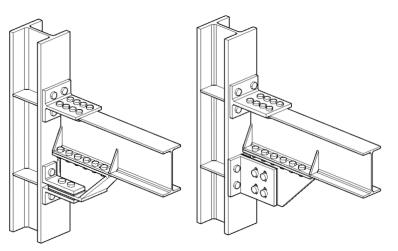
Background:

Introduction of partial-strength friction joints

This type of joints are widely used in New Zealand. Clifton and MacRae developed the so-called sliding hinge joints.

In Europe, these types of joints have been recently prequalified in the RFCS FREEDAM project.

Thanks to the ongoing dissemination project **FREEDAM Plus**, all rules and requirements are available.



FREEDAM PROJECT

- Leader: University of Salerno
- University of Naples "Federico II"
- PARTNER
- University of Liege
 - University of Coimbra
 - FIP
 - O FELIZ







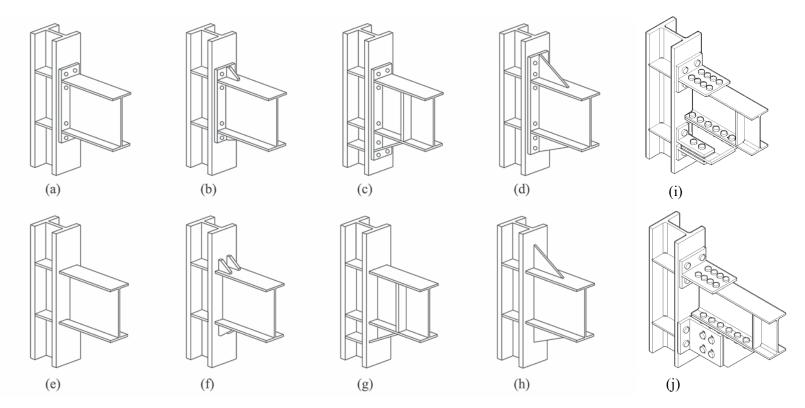






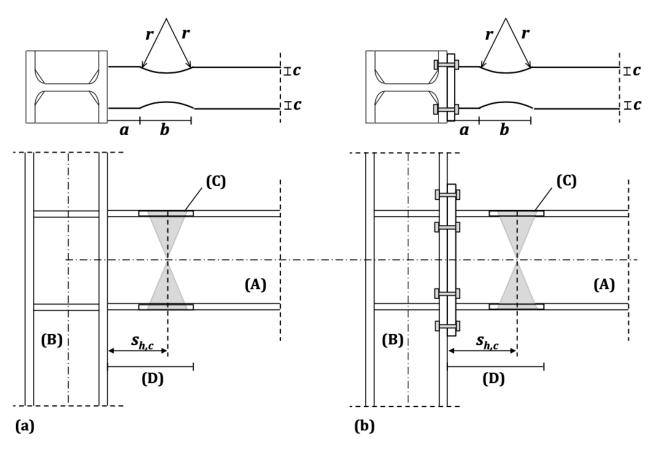


Types of beam-to-column joints covered by Annex E



unstiffened (a, e), stiffened wth ribs (b, d, f, h), stiffened with haunches (c, g), friction joint parallel to the beam flange (i) friction joint parallel to the beam web (j)

Types of beam-to-column joints covered by Annex E

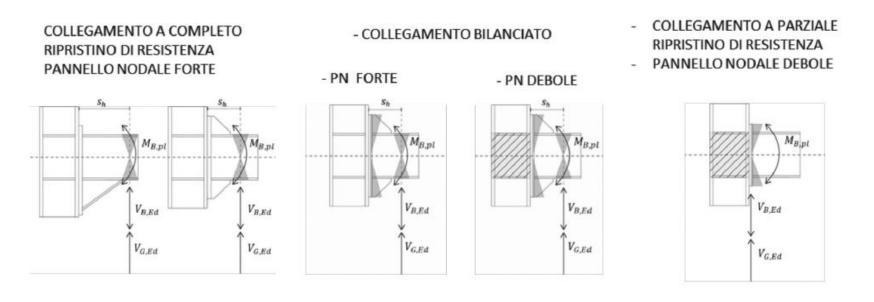


Joints with reduced beam section

Moment resisting beam-to-column joints

Classification by localization of dissipative mechanism in the joint:

The categories of the connections are classified on the basis of the localization of the dissipative mechanism in the joint:



Gusset plate connections in concentrically bracings

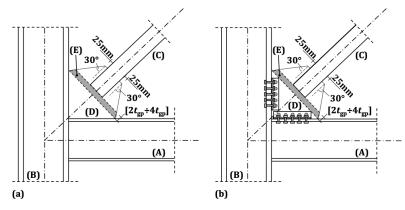


Figure E.18 — Configurations of gusset plate connections for out-of-plane buckling: a) welded connection; (b) bolted connection; (b) bolted connection; (A) beam; (B) column; (C) diagonal brace; (D) gusset plate; (E) linear clearance

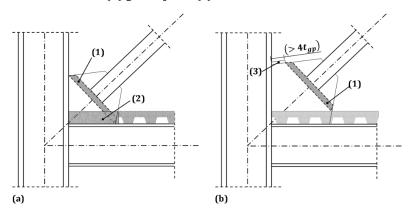


Figure E.19 — slab-to-gusset details: a) isolated from the slab; (b) restrained by the slab; (1) linear clearance; (2) compressible material; (3) edge stiffener

Brace connections in eccentric bracings

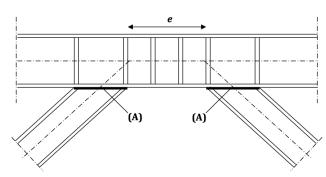
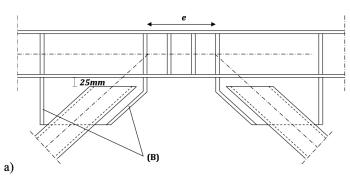


Figure E.25 — Welded brace connections of EBF: (A) full penetration groove welds in accordance with E.3.3.3(6)



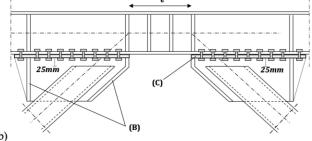
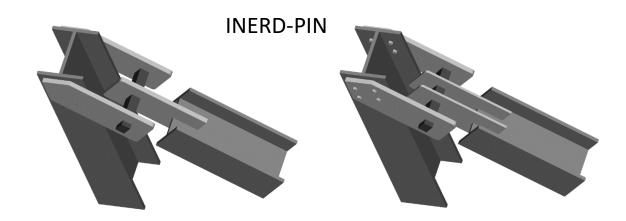


Figure E.26 — Gusset plate connections of diagonal braces of EBF: (B) stiffeners of the free edge of the gusset; (C) end-plate connection in bolted gusset plates

Partial strength connections in concentrically bracings



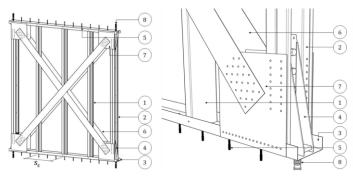
- The INERD-PIN connection is made of a pin that crosses two external plates connected to the frame columns/beams, and one or two internal plates connected to the brace
- Limits for beams and columns (geometry and material)
- Rules for welds, bolts, stiffeners, gussets (geometry and material)
- Rules for calculation of strength and modelling

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ANNEX F Complementary design rules for Lightweight steel structures

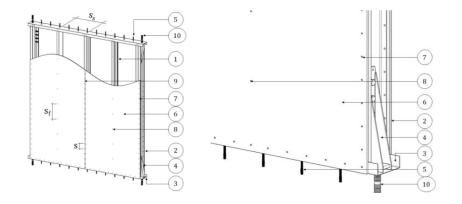
Annex F: Complementary rules for lightweight structures

Types of systems covered by Annex F

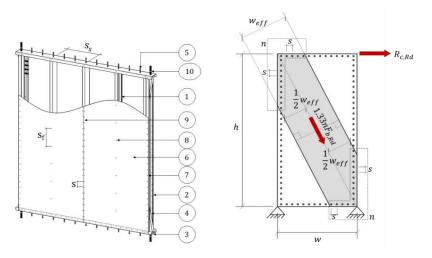


Strap braced walls

- Limits for elements (geometry and material)
- Rules for fasteners (geometry and material)
- Rules for calculation of strength and modelling



Shear walls with wood or gypsum sheathing



Shear walls with steel sheet sheathing

Annex F: Complementary rules for lightweight structures

Design of non-dissipative components for DC2 dissipative lightweight steel systems

(1) In DC2, non-dissipative components should be designed to resist the action effect E_{Ed} calculated with Formula (11.54):

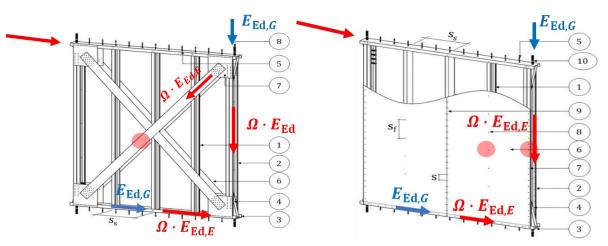
$$E_{\rm Ed} = E_{\rm Ed,G} " + " \Omega E_{\rm Ed,E}$$
 (11.54)

where:

 $E_{\rm Ed,G}$ is the action effect due to the non-seismic actions in the seismic design situation;

 $E_{\rm Ed,E}$ is the seismic action effect due to the design seismic action;

 Ω is the seismic action magnification factor, see Table 11.6.

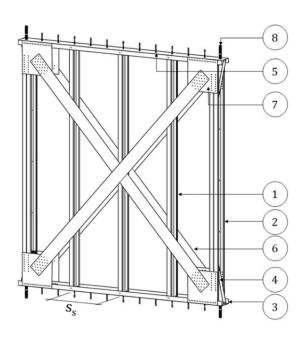




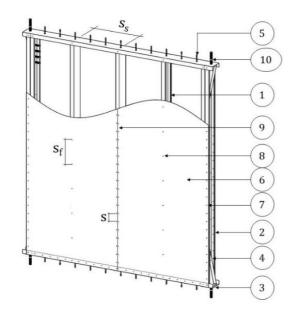
LFRS	DC2
	Ω
Strap-braced walls	1.5
Shear walls with steel	1.5
sheet sheathing;	1.5
Shear walls with wood	1.5
sheathing	1.5
Shear walls with gypsum	1.3
sheathing	1.3

Annex F: Complementary rules for lightweight structures

Design of non-dissipative components for DC3 dissipative lightweight steel systems



$$E_{\it Ed} = E_{\it Ed,G}$$
 "+" 1,1 · $\omega_{\it rm}$ · $E_{\it Nfy}$ $E_{\it Ed} = E_{\it Ed,G}$ "+" k · $E_{\it Rc,Rd}$



$$E_{Ed} = E_{Ed,G} "+ "k \cdot E_{Rc,Rd}$$

Design of non-dissipative component in Strap braced wall and Shear wall in DC3

ANNEX H Seismic design of exposed and embedded steel and composite column base connections

Annex H: Seismic design of exposed and embedded steel and composite column base connections

Use of this informative Annex

This Informative Annex provides complementary / supplementary guidance to 11 and 12.

Scope

This annex can be used for the design of column base connections retaining moment in steel and/or composite steel - concrete buildings.

NOTE: Free to rotate column bases are not covered by this Annex.

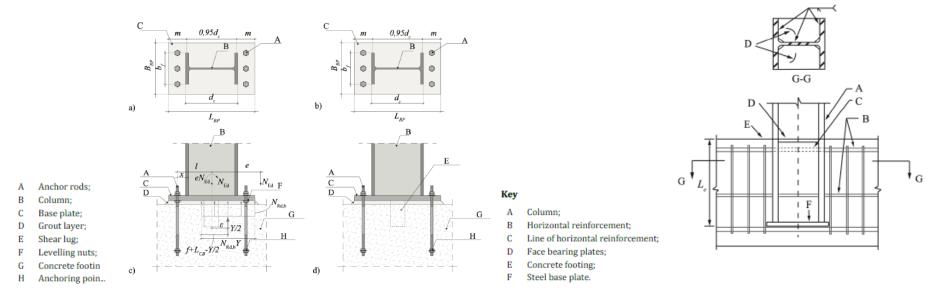


Figure H.1 — Schematic representation of exposed column base connection

Figure H.3 — Typical embedded column base connection detail

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- Introduction
- Specific rules for steel buildings
- Specific rules for composite steel-concrete buildings
- Specific rules for aluminum buildings
- Conclusions

EC8 1st Generation

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EC8 2nd Generation



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EN1998-1 (2004) – Chapter 7 Chapter 7 of EN1998-1 has 26 pages

EN1998-1-2 (2025) – Chapter 12 Chapter 12 of EN1998-1-2 has 27 pages

Evolution of seismic rules

STEEL CHAPTER EC8 1ST GENERATION EN 1998-1 (2005) Chapter 7 VS

EC8 2ND GENERATION EN 1998-1-2 (2025) Chapter 12

- Introduction of new design rules for low-moderate/medium ductility (DC2);
- Introduction of new structural types;
- Improvement of seismic design rules for traditional types;
- New Annexes





EN1998-1 (2004) - Chapter 7

Annex C - DESIGN OF THE SLAB OF STEEL-CONCRETE COMPOSITE BEAMS AT BEAM-COLUMN JOINTS IN MOMENT RESISTING FRAMES EN 1998-1-2 (2025) Chapter 12

I - DESIGN OF THE SLAB OF STEEL-CONCRETE COMPOSITE BEAMS AT BEAM-COLUMN JOINTS IN MOMENT RESISTING FRAMES

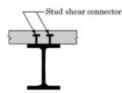
G - DESIGN OF COMPOSITE CONNECTIONS IN DISSIPATIVE COMPOSITE STEEL-CONCRETE MOMENT RESISTING FRAMES

> H - SEISMIC DESIGN OF EXPOSED AND EMBEDDED STEEL AND COMPOSITE COLUMN BASE CONNECTIONS

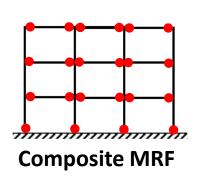
I nuovo standard europeo per la progettazione sis

Specific rules for composite steel-concrete buildings

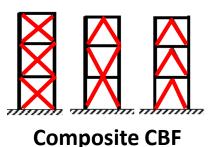
Basis of Design: Structural Types



Frames with composite members



- Steel or composite beams and/or columns
- Full or partial strength connections
- Plastic hinges can form at the ends of the beams and at the bases of the ground columns or in the connections.
- Steel dissipative beams: chapter 11
- Composite dissipative beams: chapter 12
- Steel joints: Annex E to Ch. 11
- Composite joints: annex G to Ch. 12



- Steel or composite beams and/or columns
- Braced steel of filled composite
- Dissipative zones are located in the diagonal members
- Steel dissipative braces: chapter 11
- Composite dissipative braces: chapter 12

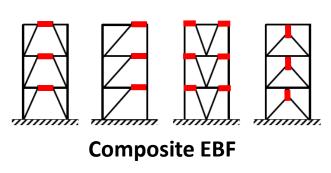
Il nuovo standard europeo per la progettazione sismica

Specific rules for composite steel-concrete buildings

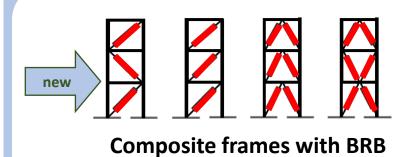
Basis of Design: Structural Types

Stud shear connector

Frames with composite members

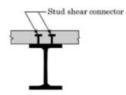


- Members not containing seismic links may be steel or composite
- Dissipative zone are located in the link
- Steel dissipative links: chapter 11

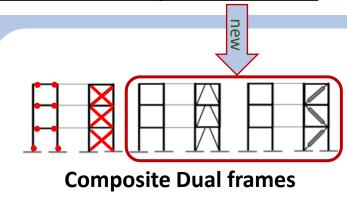


- Steel or composite beams and/or columns
- Dissipation energy takes place in the BRBs
- Design of BRBs: chapter 11

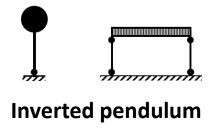
Basis of Design: Structural Types



Frames with composite members



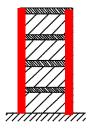
- Beams and/or columns may be steel or composite
- Bracings may be steel or filled composite
- Dissipatation energy takes place both in the bracings and MRF part
- Steel dissipative members: chapter 11
- Composite dissipative members: chapter 12



- Steel or composite beams and/or columns
- Dissipation of energy takes place mainly at the base of a single building element or at the bases of columns.
- Steel dissipative members: chapter 11
- Composite dissipative members: chapter 12

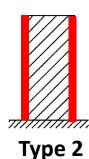
Basis of Design: Structural Types

Composite structural wall systems



Steel or composite moment frames with connected concrete infill panels

- Dissipatation energy takes place in the vertical steel sections and in the vertical reinforcement
- Type 1
- Composite dissipative vertical members: chapter 12

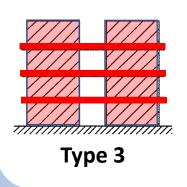


Composite walls reinforced by connected encased steel sections

- Dissipatation energy takes place in the vertical steel sections and in the vertical reinforcement
- Composite dissipative vertical members: chapter 12

Basis of Design: Structural Types

Composite structural wall systems



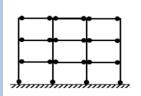
Composite of concrete walls coupled by steel or composite beams

- Type 3 composite structural wall systems should be designed to dissipate energy in the shear walls and in the coupling beams.
- Steel dissipative coupling beams: chapter 11
- Composite dissipative coupling beams: chapter 12
- Concrete shear walls: chapter 10

Basis of Design: Structural Types

Frames with dissipative composite members:

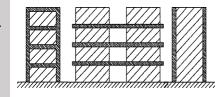
- Composite MRF
- Composite braced frames
- Composite frames with BRBs
- Composite Dual systems
- Composite inverted pendulum



- Design objectives and global rules are common to those for steel systems, and they are given in Chapter 11
- Local rules and technological requirements for composite members are given in Chapter 12

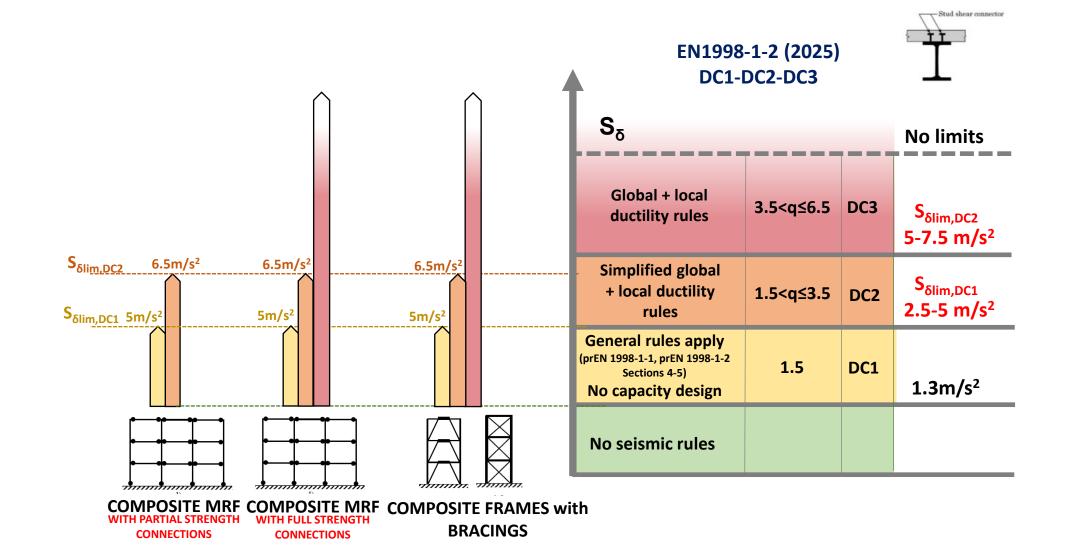
Composite structural wall systems

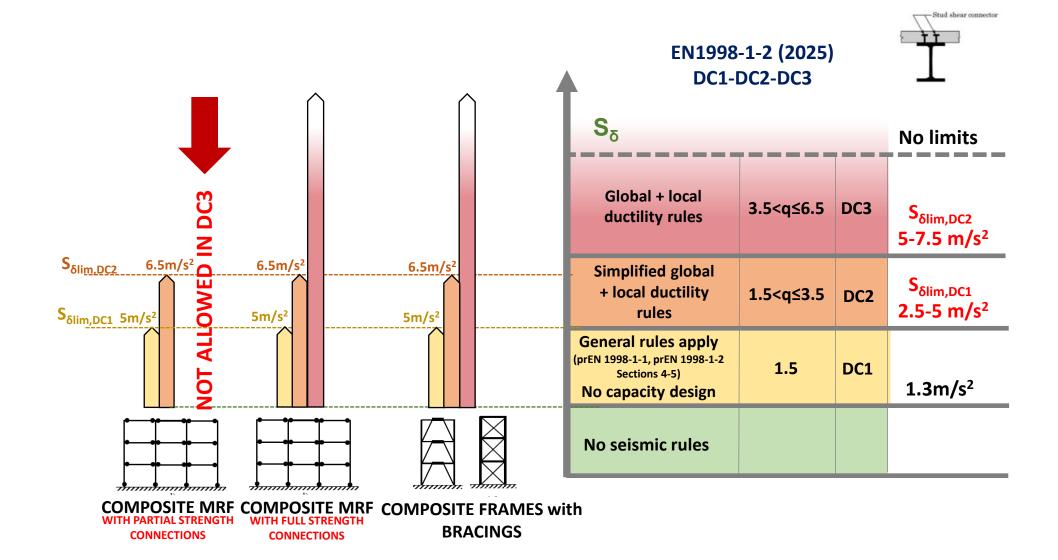
- Steel or composite moment frames with connected conrete infill panels
- Composite walls reinforced by connected encased steel sections
- Composite of concrete walls coupled by steel or composite beams



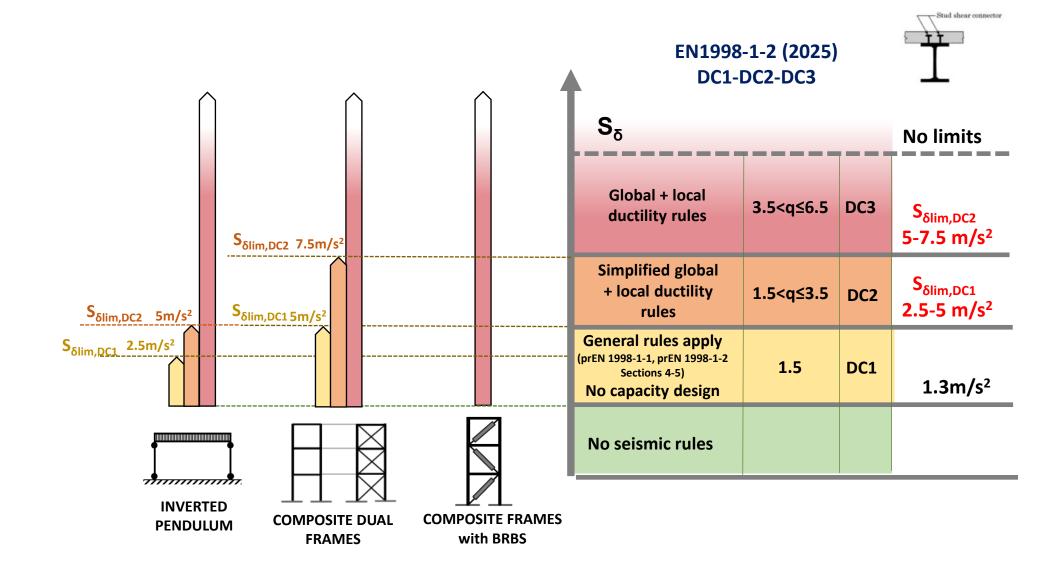
- Design objectives and global rules are given in Chapter 12
- Local rules and technological requirements for composite members are given in Chapter 12

Specific rules for composite steel-concrete buildings

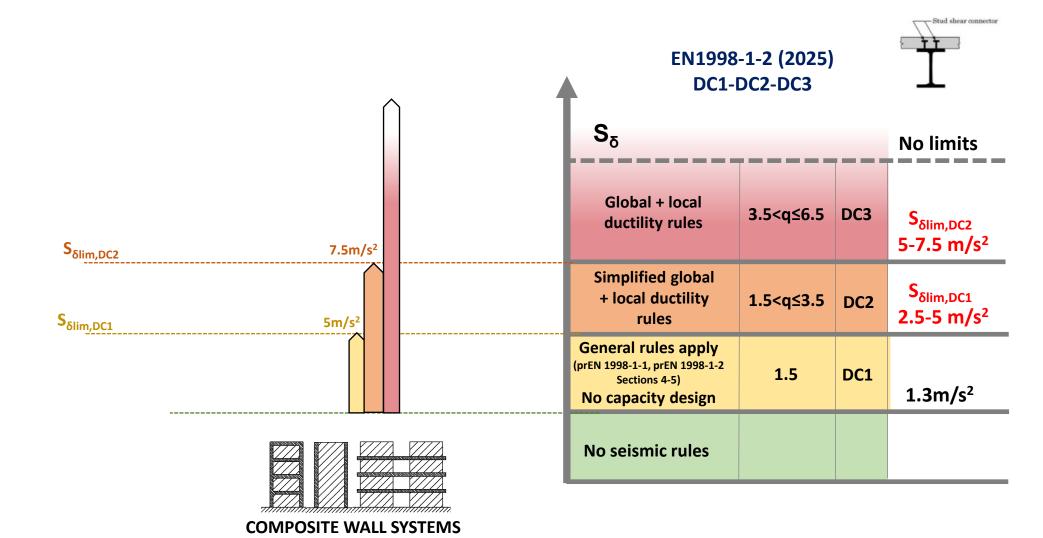




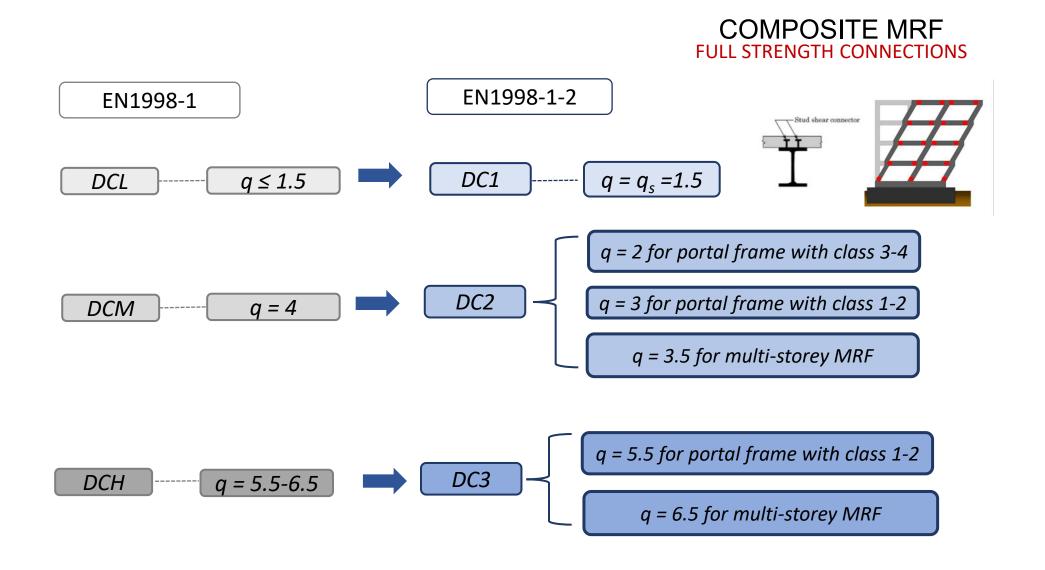
Specific rules for composite steel-concrete buildings



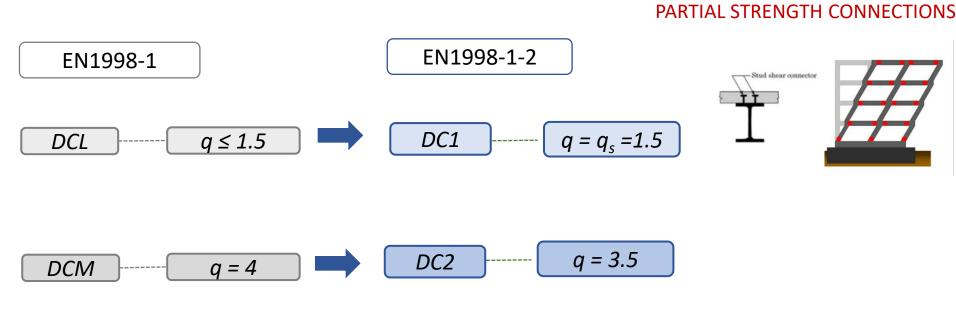
Specific rules for composite steel-concrete buildings



Specific rules for composite steel-concrete buildings

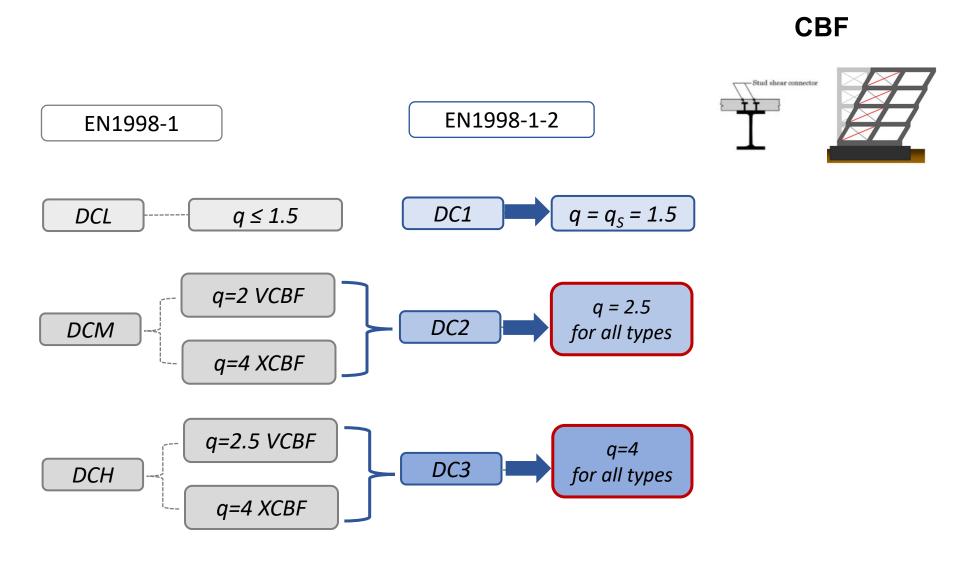






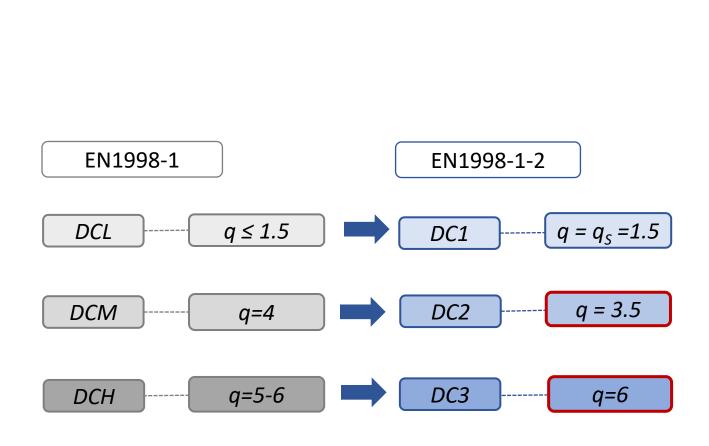
$$DCH \longrightarrow DC3$$
 NOT ALLOWED

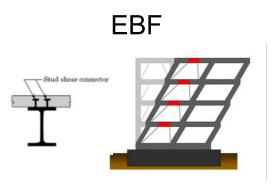
Specific rules for composite steel-concrete buildings



Il nuovo standard europeo per la progettazione sismica

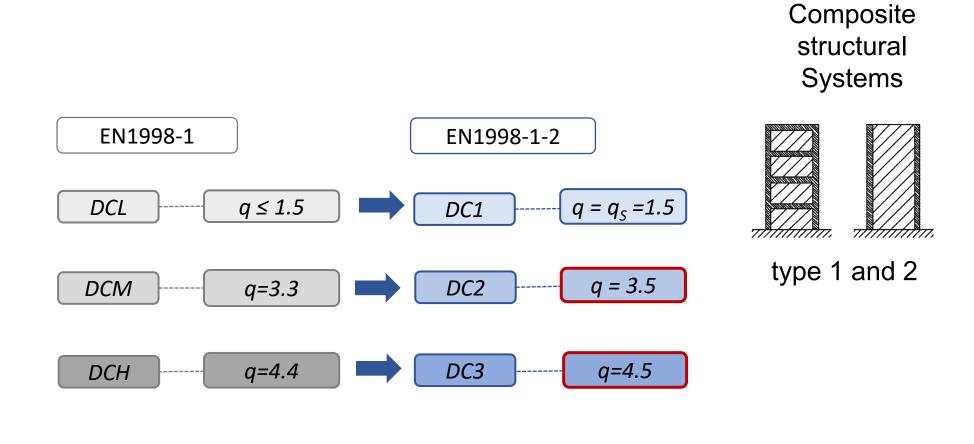
Specific rules for composite steel-concrete buildings





Il nuovo standard europeo per la progettazione sismica

Specific rules for composite steel-concrete buildings

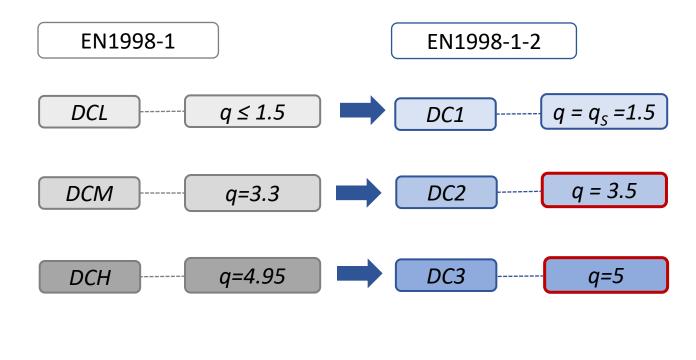


^{*} α_u/α_1 =1.1

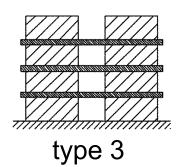
I nuovo standard europeo per la progettazione sismica

Specific rules for composite steel-concrete buildings

Basis of Design: behaviour factors



Composite structural Systems



^{*} α_{ν}/α_{1} =1.1

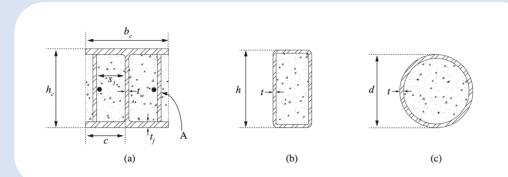
Basis of Design: local slenderness limit

Local slenderness limits for composite members



EN-1998-1 (2004)

$$\varepsilon = \left(235/f_{\rm y}\right)^{0.5}$$



Ductility class	DCM		DCH
Reference value of behaviour factor	q = 1,5-2	$1.5 - 2 < q \le 4$	q > 4
Partially or fully encased H- or I-cross section: $c/t_{\rm f}$ limits:	20ε	14ε	9ε
Filled rectangular cross section: h/t limits:	52ε	38ε	24ε
Filled circular cross section: d/t limits:	$90\varepsilon^2$	$85\varepsilon^2$	$80\varepsilon^2$

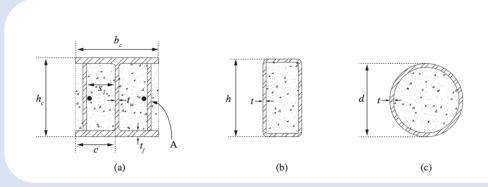
Basis of Design: required cross sectional classes

Local slenderness limits for composite members



EN 1998-1-2 (2025)

$$\varepsilon = \left(235/f_{\rm y}\right)^{0.5}$$



Ductility class	DC2		DC3
Reference value of behaviour factor	q = 1,5	$1,5 < q \le 3,5$	q > 3,5
Partially or fully encased H- or I-cross section: c/t_f limits:	20ε	14arepsilon	9ε
Filled rectangular cross section: h/t limits:	70ε	52ε	35ε
Filled circular cross section: d/t limits:	$125\varepsilon^2$	$90\varepsilon^2$	$80\varepsilon^2$

SLIGHTLY LESS STRINGENT

Structural analysis: drift limitation

Verification of drift

EN-1998-1 (2004)

At Damage Limitation state the interstorey drift should be verified as follows

$$d_r \leq \alpha h$$

where $\alpha = 0.005$; 0.0075; 0.01 depeding on the non–structural elements

EN-1998-1-2 (2025)

No mandatory check at Damage Limitation.

At Significant Damage limit state should be verified as follows:

$$d_r \leq \lambda h$$

where λ = 0.01; 0.015; 0.017; 0.02 depeding on the structural system

Capacity design: general rules

Capacity design rules: DCM VS DC2

EN-1998-1 (2004) DCM and DCH

$$R_d \ge E_{Ed,G} + 1.1 \cdot \gamma_{ov} \cdot \Omega \cdot E_{Ed,E}$$

$$\Omega = \min \left(\frac{R_d}{E_{Ed}} \right)$$

EN-1998-1-2 (2025) DC2

$$M_{Rd} \ge M_{Ed,G}" + "M_{Ed,E}$$

$$V_{Rd} \ge V_{Ed,G}" + "V_{Ed,E}$$

$$N_{Rd} \geq N_{Ed,G}" + "\Omega \cdot N_{Ed,E}$$

$$\Omega =$$
from the Table 12.5

In current DCM all seismic induced effects are magnified
In new DC2 only axial forces are magnified

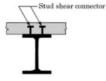


Table 12.5 — Members to which (1) or (2) should be applied. Values of seismic action magnification factor Ω for structural types in DC2

Structural types	$oldsymbol{arOmega}$	Members
Composite moment resisting frames (CMRFs): With full-strength connections	See Table 11.7	Columns
With partial-strength connections	2,0	Columns
Composite frames with concentric bracings	See Table 11.7	Beams and columns
Composite frames with eccentric bracings	See Table 11.7	Beams outside the link, braces and columns
Composite inverted pendulum structures	See Table 11.7	Columns
Composite dual frames CMRFs with concentric bracings CMRFs with eccentric bracings	See Table 11.7	Beams and columns of the concentric bracing; columns of the CMRF Beams outside the link, braces and oclumns of the eccentricl bracing; columns of the CMRF
Composite structural wall systems	2.0	None
Types 1, 2 and 3	2,0	None

Capacity design: general rules

Capacity design rules: DCH VS DC3

EN1998-1 (2004) DCM and DCH

$$R_d \ge E_{Ed,G} + 1.1 \cdot \gamma_{ov} \cdot \Omega \cdot E_{Ed,E}$$

$$\Omega = \min \left(\frac{R_d}{E_{Ed}} \right)$$

EN1998-1-2 (2025) DC3

$$R_d \ge E_{Ed,G} + \omega_{rm} \cdot \omega_{sh} \cdot \Omega_d \cdot E_{Ed,E}$$

$$\Omega_d = \min\left(\frac{R_d}{E_{Ed,E}}\right)$$

 ω_{sh} From Table 11.8

 ω_{rm} material randomness coefficient

In new DC3 the hardening factor is specified per dissipative mechanism

Table 11.8 — Overstrength factor $\omega_{\rm sh}$ accounting for hardening of the dissipative zones

Structural Type	Dissipative Zones	Plastic Mechanism	$\omega_{ m sh}$
Moment resisting frames	beams yielding connections columns at base	bending	$\frac{\left(f_{y}+f_{u}\right)}{2f_{y}}\leq1.2$
	friction connections	friction	$1.3\omega_{\rm sr}\omega_{\mu} \leq 2.2$ $\omega_{\rm sr}$ and ω_{μ} as defined in Annex E
Frames with concentric	diagonal members	axial	1,1
	all members	bending (see 11.10.5 and 11.10.6)	1,1
bracings (simple and dual)	dissipative	axial	1,1
	connections	bending	1,2
		shear	1,5
	short links	shear $e \leq M_{\rm p,link}/V_{\rm p,link}$ (very short links)	1,8
		shear $M_{\rm p,link}/V_{\rm p,link} \le e \le 1,6 M_{\rm p,link}/V_{\rm p,link}$ (short links)	1,5
Frames with eccentric	intermediate links	bending and shear $e \le 2.6M_{\rm p,link}/V_{\rm p,link}$	1,5
bracings (simple and dual)		bending and shear $2.6M_{\rm p,link}/V_{\rm p,link} \le e \le 3M_{\rm p,link}/V_{\rm p,link}$	1,35
		Bending $3M_{\rm p,link}/V_{\rm p,link} \le e \le 5M_{\rm p,link}/V_{\rm p,link}$	1,25
	long links	Bending $e > 5M_{\rm p,link}/V_{\rm p,link}$	$\omega_{\rm sh} = \frac{\left(f_{\rm y} + f_{\rm u}\right)}{2f_{\rm y}} \le 1.2$
	beams - columns	bending (see 11.11.5)	1,1
Frames with buckling restrained braces	diagonal members	axial	see 11.12.3(4)
restrained braces	beams - columns	bending (see 11.12.6)	1,2

Additional rules and technological requirement for composite members

- Composite steel Beams with slab
- Lateral torsional restraint

BEAM

COLUMN

• Shear connection grade

- Slab effective width for plastic reistance (b_{eff})
- Ductility of composite beam with slab (zc/dc)
- Seismic rebar
- Condition for disregarding the composite action of beams with slab
- Encased columns
- Length and location of critical regions
- Spacing s of confining hoops within critical regions
- Diameter of the hoop
- Distance between consecutive longitudinal bars
- Partially-encased columns
- Detail of welding of longitudinal bars to straigth links
- Diameter of straigth links
- Clear concrete cover of straigth links
- Filled columns
- Reinfocing steel contribution ratio
- Shear resistance of dissipative and non-dissipative filled composite columns.
- Connections NEW ANNEXES G, H

Small differences between EN 1998-1 (2004) and EN 1998-1-2 (2025)

Annex G DESIGN OF COMPOSITE CONNECTIONS IN DISSIPATIVE COMPOSITE STEEL-CONCRETE MOMENT RESISTING FRAMES

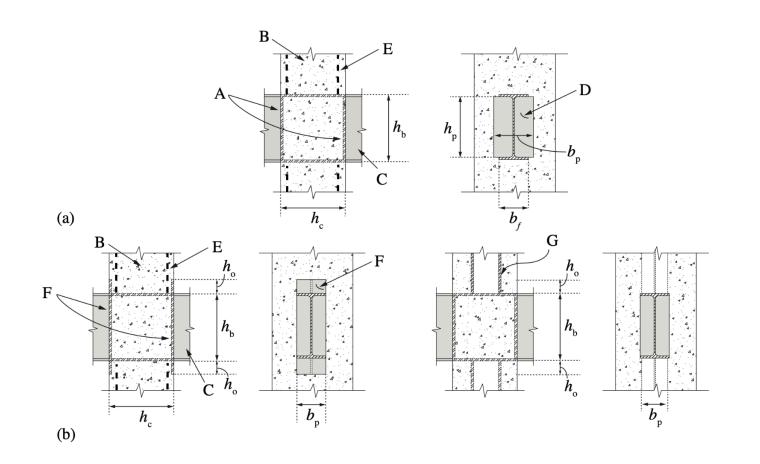
Scope

This annex should be used for the design, fabrication and quality criteria of **full-strength composite connections** of dissipative composite steel or steel beams to composite or concrete columns in composite steel - concrete moment resisting frames designed to DC2 and DC3.

Annex G: Design of composite connections in dissipative

composite steel-concrete moment resisting frames

Joints between steel beams and reinforced concrete or composite columns



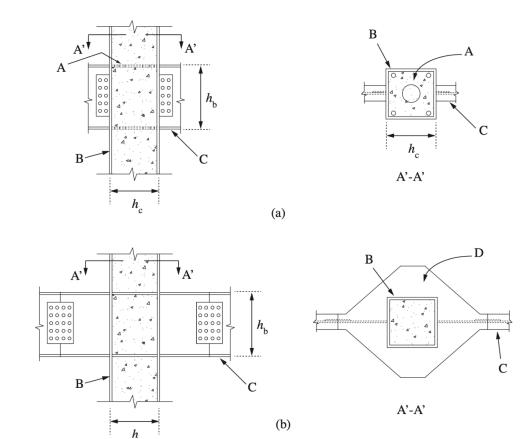
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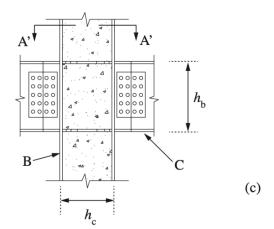
- A Face bearing plates;
- B Column;
- C Steel or composite beam;
- D Wide face bearing plate;
- E Vertical reinforcement bars;
- F Extended face bearing plates;
- G Structural steel profile;

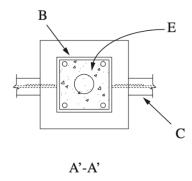
Annex G: Design of composite connections in dissipative

composite steel-concrete moment resisting frames

Composite joints using diaphragm plates







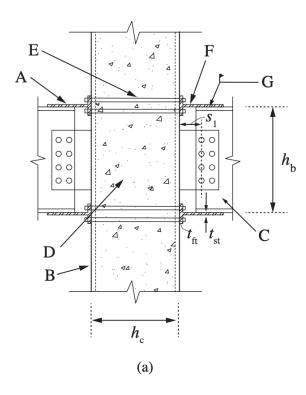
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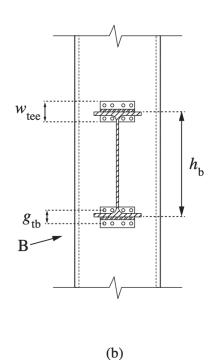
- A Internal diaphragm plate;
- B Concrete-filled tube;
- C I-shape beam;
- D External diaphragm plate;
- E Through diaphragm plate.

Annex G: Design of composite connections in dissipative

composite steel-concrete moment resisting frames

Full-strength composite joints with double-split tee connections in concrete filled tube columns





- A Tee-stub;
- B Concrete-filled tube;
- C Steel beam;
- D Web panel joint;
- E Structural bolt;
- F Compressive length of tee-stub;
- G Fillet weld of tee-stub to the steel beam flange.

Contents

- Introduction
- Specific rules for steel buildings
- Specific rules for composite steel-concrete buildings
- Specific rules for aluminum buildings
- Conclusions

Specific rules for aluminium buildings

Background

The most of rules about materials, connections and hiearchy are derived from Japanese seismic recommendantions on Aluminum structures

告 修 国土交通省国土技術政策総合研究所 国立研究開発法人建築研究所

アルミニウム建築 構造設計規準・同解説

平成15年5月制定平成28年3月改訂

平成28年3月

アルミニウム建築構造協議会
一般社団法人日本アルミニウム協会

Evolution of seismic rules

ALUMINUM CHAPTER EC8 1ST GENERATION NO SEISMIC RULES

VS

EC8 2ND GENERATION EN 1998-1-2 (2025) Chapter 15

- Introduction of new seismic design rules for aluminum structures missing in the previous EC8
- Japanese seismic code constituted the background for new seismic design procedure
- Design rules solely for DC2 are provided.

MAIN NOVELTIES

EC8 2nd Generation

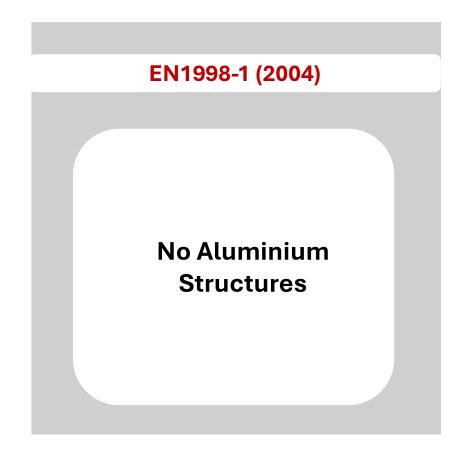
CHAPTER 15:

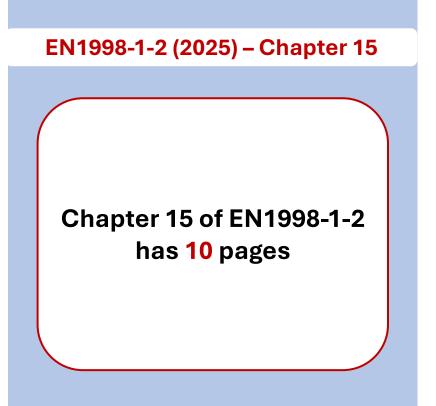
SPECIFIC RULES FOR ALUMINIUM BULDINGS

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Specific rules for steel buildings





Il nuovo standard europeo per la prodettazione s

Specific rules for aluminium buildings

Basis of Design: Structural Types

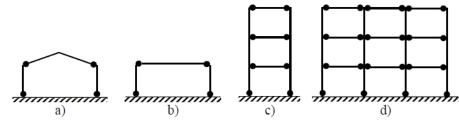
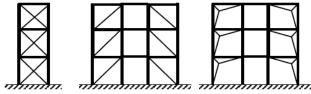


Figure 11.1 — Moment resisting frames (dissipative zones in beams and at bottom of columns): a) portal frame; b) single-storey MRF; c) single-span multi-storey MRF; d) multi-span multi-storey MRF



 $\begin{tabular}{ll} Figure~11.2-Frames~with~concentric~bracings~where~the~concept~of~tension-only~diagonals~is~allowed \\ \end{tabular}$

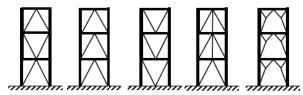
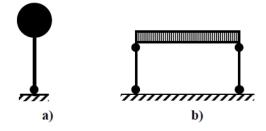


Figure 11.3 — Frames with concentric bracings where the concept of tension-compression diagonals is mandatory



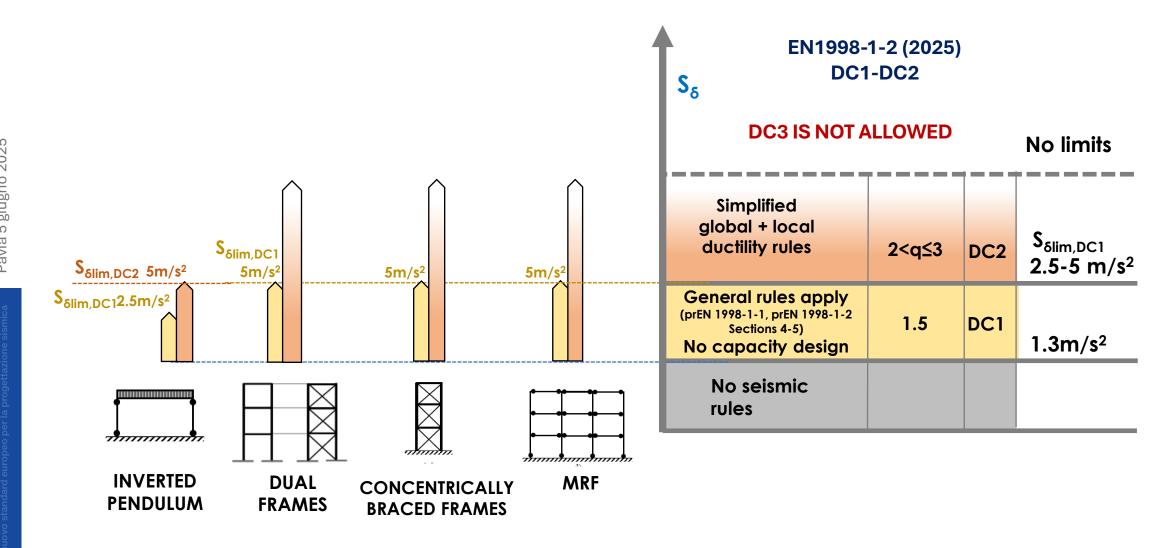
Figure 11.6 — Dual frames with moment resisting frame combined with either concentric, eccentric or buckling restrained bracing (dissipative zones in both moment and braced frames)



igure 11.8 — Inverted pendulum: a) dissipative zones at the column base; b) dissipative zones in columns $(N_{\rm Ed,G}/N_{\rm pl,Rd} \ge 0.3)$

EBFS ARE NOT ALLOWED

Basis of Design: limits of seismic action



Pavia 5 giugno 2025

Basis of Design: behaviour factors

	Du	ctility Cl	ass
STRUCTURAL TYPE	DC2		
	$q_{ m D}$	$q_{ m R}$	q
Moment resisting frames (MRFs)			
Single-storey MRFs	1,5	1,1	2,5
Multi-storey MRFs	1,5	1,3	3,0
Frames with concentric bracings			
Diagonal bracings	1 🗗	1.0	2.2
V-bracings	1,5	1,0	2,3
X-bracings on either single or two-storey			
Dual frames (MRFs with concentric bracing)	1,7	1,2	3,0
Inverted pendulum	1,3	1,0	2,0

Material

ER/B- Extruded rod and bar

Permitted alloys and temper for dissipative parts in DC2

Structural element	Product form	alloy	temper	thickness
		5052	H12 H22/H32	≤40
	-	5049	0/H111	≤100
		5083	0/H111	≤80
		5383	0/H111	≤120
Sheet, strip and plate		5565	H116/H321	≤80
		5454	0/H111	≤80
		5754	0/H111	≤100
		6061	T4 / T451	≤12,5
		6082	T4 / T451	≤12,5
	ET,EP,ER/B	5083	O/H111 F/H112	≤200
	ET,EP,ER/B	5454	O/H111 F/H112	≤25
Extruded profiles, extruded	ET,EP,ER/B	5754	O/H111 F/H112	≤25
tube, extruded rod/bar and drawn tube	DT	(0(0	Т6	≤20
urawii tube	EP,ET,ER/B	6060	T64	≤15
	EP,ET,ER/B	6061	T4	≤25
	DT		Т4	≤20
	EP,ET,ER/B	6082	Т4	≤25
Legend:				
P- Extruded profiles ET- Extruded tube				

DT- Drawn tube

Alloys different from those specified in Table 15.2 may be used, provided that the ratio f_u/f_0 is not smaller than 1,10 and the elongation at failure is not smaller than 10%

where $\mathbf{f_u}$ is the ultimate tensile strength and $\mathbf{f_0}$ is the conventional elastic strength

Structural analysis: second order effects and drift limitation

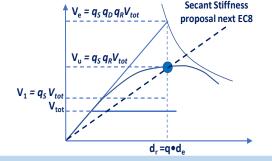
Deformation-related requirements

Second order effects

Modified stability coefficient based, which account for design overstrength and

the plastic distribution

$$\theta = \frac{P_{tot} \cdot d_r}{q_s \cdot q_R \cdot V_{tot} \cdot h}$$



Interstorey drift

The interstorey drift at SD limit state should be limited to:

- a) $d_{r,SD} \le 0.02 h$ for moment frames;
- b) $d_{r,SD} \le 0.015 h$ for frames with concentric bracings, for dual frames and inverted pendulum structures;

Capacity design: general rules

For aluminum systems DC2 all seismic induced effects are magnified

EN1998-1-2 (2025) DC2

$$M_{Rd} \ge M_{Ed,G}" + "\Omega \cdot M_{Ed,E}$$

$$V_{Rd} \ge V_{Ed,G}" + "\Omega \cdot V_{Ed,E}$$

$$N_{Rd} \ge N_{Ed,G}" + "\Omega \cdot N_{Ed,E}$$

$$\Omega = \text{ from the Table 15.5}$$

Capacity design: general rules

Table 15.5 — Members to which (1) apply. Values of seismic action magnification factor Ω in DC2

STRUCTURAL TYPE	Ω	Members to which (1) apply		
Moment resisting frames (MRFs)				
Single-storey MRFs	1,8	aalumna		
Multi-storey MRFs	2,0	columns		
Frames with concentric bracings				
Diagonal bracings	1,5	beams and columns		
V-bracings	1,5			
X-bracings on either single or two-storey				
Dual frames (MRFs with concentric bracing)	2,0	beams and columns of the concentric bracing; columns of the MRF		
Inverted pendulum	1,5	columns		

Capacity design: general rules

Rules for connections in dissipative zones

The general rules for non dissipative connections is similar to the steel structures, namely:

$$R_d \geq \omega_{rm} \cdot \omega_{sh} \cdot R_{fo}$$

where:

R_d is the resistance of the connection in accordance with EN 1999-1-1;

R_{fo} is the plastic resistance of the connected dissipative member evaluated in the expected position of the plastic hinge and based on the nominal conventional elastic strength of the material as defined in EN 1999-1-1;

 ω_{rm} is the overstrength factor accounting for variability of f_0 in the dissipative zones. In absence of experimental characterization of the material in the dissipative zones, ω_{rm} can be assumed equal to 1.5;

 $\omega_{\rm sh}$ is the overstrength factor accounting for the hardening in the dissipative zones.

 ω_{sh} =1.3 For elements in plastic bending, or the value calculated in accordance with Annex L of EN1999-1-1, whichever is greater;

 ω_{sh} =1.5 For elements in plastic tension: as 1,5 or the ratio $\frac{f_u}{f_o}$, whichever is greater

Contents

- Introduction
- Specific rules for steel buildings
- Specific rules for composite steel-concrete buildings
- Specific rules for aluminum buildings
- Conclusions

Conclusions

- The new Eurocode 8 is significantly changed as respect to the current EN1998-1(2004) regarding both general (EN 1998-1-1) and new buildings (EN 1998-1-2) rules;
- With reference to steel, steel-concrete composite and aluminum structures, the contribution provided by the joint committee SC8/WG2-ECCS/TC13 was fundamental, and it provided the scientific background for all the proposed changes;
- The new Chapter (11) on steel structures and Chapter (12) on steel-concrete composite structures are significantly improved and more complete: many criticisms have been eliminated, as well as new structural types, such as the BRB and light structures, have been included. The introduction of seismic prequalification of beam-to-column joints represents one of the most important novelties;
- The new Chapter (15) on aluminum structures is one of the major novelties of EN19981-2 (2025), being the first set of rules in Europe for seismic design of aluminum structures;
- In the near future, wide use of the new rules is expected, by application in both scientific and professional communities.







Materiali e tipologie costruttive

EN1998-1-2. Strutture metalliche e composte acciaio-cls

Thank You

for your kind attention

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